

Technical Report CERC-93-9 June 1993

Annual Data Summary for 1991 CERC Field Research Facility

Volume I: Main Text and Appendixes A and B

by Michael W. Leffler, Clifford F. Baron, Brian L. Scarborough, Kent R. Hathaway Coastal Engineering Research Center



Approved For Public Release; Distribution Is Unlimited

93'8 26 130

93-20102

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names does not constitute an official endorsement or approval of the use of such commercial products.



Annual Data Summary for 1991 CERC Field Research Facility

Volume 1: Main Text and Appendixes A and B

by Michael W. Leffler, Clifford F. Baron, Brian L. Scarborough, Kent R. Hathaway Coastal Engineering Research Center

U.S. Army Corps of Engineers Waterways Experiment Station 3909 Halls Ferry Road Vicksburg, MS 39180-6199

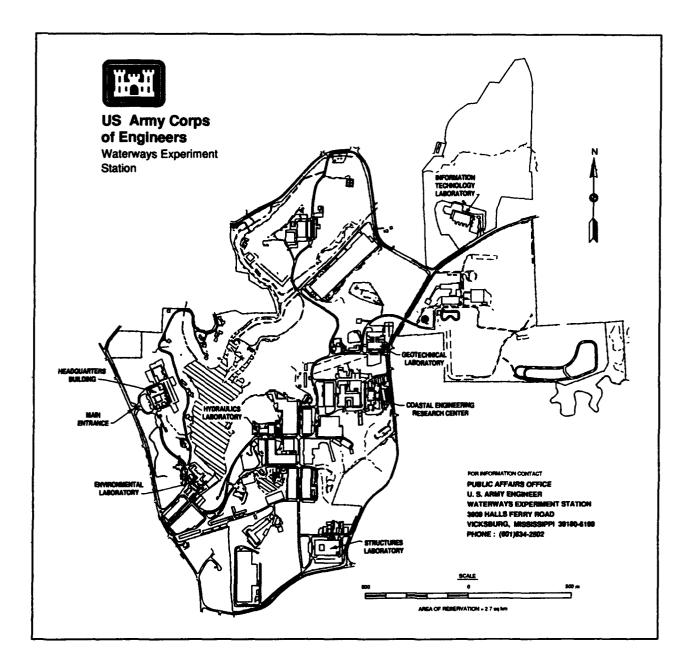
Final report

Approved for public release; distribution is unlimited

Prepared for U.S. Army Corps of Engineers

Washington, DC 20314-1000

Under FRF Analysis Work Unit 32525



Waterways Experiment Station Cataloging-in-Publication Data

Annual data summary for 1991 CERC Field Research Facility / by Michael W. Leffler ... [et al.], Coastal Engineering Research Center; prepared for Department of the Army, U.S. Army Corps of Engineers.

2 v. : ill. ; 28 cm. — (Technical report; CERC-93-9)

1. Ocean waves — North Carolina — Statistics. 2. Meteorology, Maritime — North Carolina — Statistics. 3. Oceanographic research stations — North Carolina — Duck. 4. Oceanography — North Carolina — Observations. I. Leffler, Michael W. II. United States. Army. Corps of Engineers. III. Coastal Engineering Research Center (U.S.) IV. U.S. Army Engineer Waterways Experiment Station. V. Series: Technical report (U.S. Army Engineer Waterways Experiment Station); CERC-93-9.

PREFACE

This report is the 13th in a series of annual data summaries authorized by Headquarters, US Army Corps of Engineers (HQUSACE), under Civil Works Research Work Unit 32525, "Field Research Facility Analysis," Coastal Flooding Program. Funds were provided through the US Army Engineer Waterways Experiment Station (WES), Coastal Engineering Research Center (CERC), under the program management of Ms. Carolyn M. Holmes, CERC. The HQUSACE Technical Monitors were Messrs. John H. Lockhart, Jr.; Barry W. Holliday; John G. Housley; and David A. Roellig.

Data for the report were collected and analyzed at the WES/CERC Field Research Facility (FRF) in Duck, NC. The report was prepared by Mr. Michael W. Leffler, FRF, under the direct supervision of Mr. William A. Birkemeier, Chief, FRF Group, Engineering Development Division (EDD), and Mr. Thomas W. Richardson, Chief, EDD; and under the general supervision of Dr. James R. Houston and Mr. Charles C. Calhoun, Jr., Director and Assistant Director, CERC, respectively. Mr. Kent K. Hathaway, FRF, assisted with instrumentation, and Mr. Brian L. Scarborough, FRF, assisted with data collection. Messrs. Clifford F. Baron, Stephen T. Blanchard, Matthew E. Cahur, Jonathan J. Lee, and Mohsen Alhaddad, and Mses. Judy H. Roughton and Juliana Atmadja assisted with data analysis at the FRF. The National Oceanic and Atmospheric Administration/National Ocean Service maintained the tide gage and provided statistics for summarization.

At the time of publication of this report, Director of WES was Dr. Robert W. Whalin. Commander was COL Leonard G. Hassell, EN.

DTIC QUALITY INSPECTED 3

Accession For

HTIS GRAAI

DTIC TAB

Unannounced

Justification

By

Distribution/

Availability Codes

Avail and/or

Special

CONTENTS

		Page
PREFA	ACE	1
PART	I: INTRODUCTION	5
	Background	5
	Organization of Report	6
	Availability of Data	7
PART	II: METEOROLOGY	9
	Air Temperature	9
	Atmospheric Pressure	11
	Precipitation	12
	Wind Speed and Direction	14
PART	III: WAVES	23
	Measurement Instruments	23
	Digital Data Analysis and Summarization	24
	Results	26
PART	IV: CURRENTS	39
	Observations	39
	Results	39
PART	V: TIDES AND WATER LEVELS	42
	Measurement Instrument	42
	Results	43
PART	VI: WATER CHARACTERISTICS	46
	Temperature	
		46
	Visibility	47
	Density	48
PART	VII: SURVEYS	50
PART	VIII: PHOTOGRAPHY	52
•	Aerial Photographs	52
	Beach Photographs	52
PART	IX: STORMS	59
	7-9 January 1991	60
	11-12 January 1991	61
	23 February 1991	62
	6-7 March 1991	63
	V / 1104-U11 1.7/1	0.3

29 March 1991														64
20-21 April 1991														65
18-19 May 1991														66
23 June 1991	•		•	•						•			•	67
18-19 August 1991 - "Hurricane Bob"										•				68
25 August 1991														69
1-2 September 1991														70
20 September 1991														71
3 October 1991														72
16-17 October 1991														73
28 October - 1 November 1991														74
8-10 November 1991														76
19 December 1991														77
31 December 1991														78
	•	•		•		•	•	•	•	•	•	•	-	
REFERENCES														79
	•	•		•	•	•	•	•	•		•	•	•	
APPENDIX A: SURVEY DATA														A1
AIIMDIA A. BORVEI DAIA	• •	• •	•	•	•	•	•	•	•	•	•	•	•	***
APPENDIX B: WAVE DATA FOR GAGE 630		•		•				•	•		•	•	•	В1
D 21 - 11 - 1 m														В1
Daily H _{mo} and T _p	•	•	• •	٠	•	•	•	•	•	٠	•	•	•	B1
Joint Distributions of H_{mo} and T_{p} .	•	•	• •	٠	•	•	•	•	•	•	•	•	•	В1
Cumulative Distributions of Wave Height														
Peak Spectral Wave Period Distributions	•	•	• •	٠	•	•	•	•	•	•	•	•	•	B1
Persistence of Wave Heights														B2
Spectra	•	•		•	•	•	•	•	•	•	•	•	•	В2
APPENDIX C*: WAVE DATA FOR GAGE 111										•			•	C1
														C1
Daily H_{mo} and T_p Joint Distributions of H_{mo} and T_p .	•	•		٠	•	•	•	•	•	•	•	•	•	C1
Joint Distributions of H_{mo} and T_{p} .	•	•	• •	•	•	•	•	•	•	•	•	•	•	C1
Cumulative Distributions of Wave Height														
Peak Spectral Wave Period Distributions														C1
Persistence of Wave Heights														C2
Spectra	•	•		•	•	•	•	•	•	•	•	•	•	C2
APPENDIX D: WAVE DATA FOR GAGE 625	•				•				•			•		D1
Daily W and T														D1
Daily H_{mo} and T_{p} Joint Distributions of H_{mo} and T_{p} .	•	•	• •	•	•	•	•	•	•	•	•	•	•	D1
Completes Distributions of Very Veicht	•	•		•	•	•	•	•	•	•	٠	•	•	DI DI
Cumulative Distributions of Wave Height														DI DI
Peak Spectral Wave Period Distributions														
Persistence of Wave Heights														D2
Spectra	•	•		•	•	•	•	•	•	•	•	•	•	D2

^{*} A limited number of copies of Appendixes C-E (Volume II) were published under separate cover. Copies are available from National Technical Information Service, 5285 Port Royal Road, Springfield, VA 22161.

APPENDIX E:	WAVE DATA FOR GAGE 645	31
Daily	H_{mo} and T_{p}	Ξ1
	Distributions of H _{mo} and T _p	
Cumula	tive Distributions of Wave Height	31
Peak S	pectral Wave Period Distributions	31
Persis	tence of Wave Heights	₹2
Spectr	a	22

ANNUAL DATA SUMMARY FOR 1991 CERC FIELD RESEARCH FACILITY

PART I: INTRODUCTION

Background

- 1. The US Army Engineer Waterways Experiment Station (WES), Coastal Engineering Research Center's (CERC's) Field Research Facility (FRF), located on 0.7 km² at Duck, NC (Figure 1), consists of a 561-m-long research pier and accompanying office and field support buildings. The FRF is located near the middle of Currituck Spit along a 100-km unbroken stretch of shoreline extending south of Rudee Inlet, VA, to Oregon Inlet, NC. The FRF is bordered by the Atlantic Ocean to the east and Currituck Sound to the west. The facility is designed to (a) provide a rigid platform from which waves, currents, water levels, and bottom elevations can be measured, especially during severe storms; (b) provide CERC with field experience and data to complement laboratory and analytical studies and numerical models; (c) provide a manned field facility for testing new instrumentation; and (d) serve as a permanent field base of operations for physical and biological studies of the site and adjacent region.
- 2. The research pier is a reinforced concrete structure supported on 0.9-m-diam steel piles spaced 12.2 m apart along the pier's length and 4.6 m apart across the width. The piles are embedded approximately 20 m below the ocean bottom. The pier deck is 6.1 m wide and extends from behind the duneline to about the 6-m water depth contour at a height of 7.8 m above the National Geodetic Vertical Datum (NGVD). The pilings are protected against sand abrasion by concrete erosion collars and against corrosion by a cathodic system.
- 3. An FRF Measurements and Analysis Program has been established to collect basic oceanographic and meteorological data at the site, reduce and analyze these data, and publish the results.
- 4. This report, which summarizes data for 1991, continues a series of reports begun in 1977.

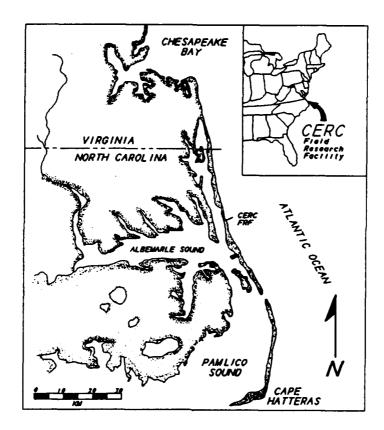


Figure 1. FRF location map

Organization of Report

- 5. This report is organized into nine parts and five appendixes.

 Part I is an introduction; Parts II through VIII discuss the various data collected during the year; and Part IX describes the storms that occurred.

 Appendix A presents the bathymetric surveys, Appendix B summarizes deepwater wave statistics, and Appendixes C through E (published under separate cover as Volume II) contain summary statistics for other gages.
- 6. In each part of this report, the respective instruments used for monitoring the meteorological or oceanographic conditions are briefly described, along with data collection and analysis procedures and data results. The instruments were interfaced with the primary data acquisition system, a Digital Equipment Corporation (Maynard, MA) VAX-11/750 minicomputer located in the FRF laboratory building. More detailed explanations of the design and the operation of the instruments may be found in Miller (1980). Readers' comments on the format and usefulness of the data presented are encouraged.

Availability of Data

7 Table 1 summarizes the available data. In addition to the wave data summaries in the main text, more extensive summaries for each of the wave gages are provided in Appendixes B through E.

Table 1
1991 Data Availability

	Gege		J	æ	i		F	ф		1	Mar	:			ψz			ŀ	by			Ju	n			Ju	L		4	Lug	3		S	p			0	ct			N	ίον	,		D	ес
	D	1	2	3	4	5	2	3	4	1	2 3	3 4	1	2	3	4	5	1 2	3	4	1	2	3	4 :	1 2	: 3	4	5	1 :	2 3	4	1	2	3	4	1	2	3	4 !	5 1	1 2	: 3	4	1	2	3
Weather							_		_								_ `			_	_											_			_					_				_		
Anemometer	932	*	*	*	*	A 1			*	1	* 1	*	*	*	*	×	* 1		*	*	*	*	×	* ,	/ *	*	*	* 1	*	* *		*	*	*	*	*	*	*	* ,	/ 1	1	*	*	*	*	*
Atmospheric Pres.	616	*	*	*	*	* 1		*	*	/	* 1	*	*	*	*	*	* 1	* 1	*	*	*	*	*	* ,	/ *	*	*	* 1	*	* 1	*	*	*	*	*	*	*	*	* ,	/ 1	• •	*	*	*	*	*
Air Temperature	624	*	*	*	*	* 1	•	*	*	/	* 1		*	*	*	*	* 1	* *	*	*	*	*	*	* ,	/ *	*	*	* 1	*	* *			*	*	-	*	*	*	*	* 1			*	*	*	*
Precipitation	604	*	*	*	*	* 1	• •	*	*	1	* 1	* *	*	*	*	*	* 1	* 1	*	*	*	*	*	* ,	/ *	*	*	* 1	*	* *	*	*	*	*	*	*	*	*	*	* 1	•	*	*	*	*	*
Waves																																														
Offshore Waverider	630	*	/	/	-			. -	-	1	* 1	*	*	*	*	*	* 1	* *	*	*	*	*	*	//	/ *	*	*	* 1	* 1	* 4	*	*	*	*	*	*	*	*	* 1	* 1		*	*	1	1	-
Pressure Gege	111	*	*	*	*	* 1		*	*	1	* 1	*	*	*	*	*	* 1	* 1	*	*	*	*	*	*	/ *	*	*	* 1	* 1	* 1	*	*	*	*	*	*	*	*	* 1			*	*	*	*	*
Pier End	625	*	*	*	*	* 1	+ +	*	*	1	* 1	*	*	*	*	*	*	* 1	*	*	*	*	*	*	/ *	*	*	* 1	•	* 1		*	*	*	*	*	*	*	* 1	* 1			*	*	*	*
Pier Nearshore	645	*	*	*	*	*	* #	*	*	1	* 1	*	*	*	*	*	* 1	* *	*	*	*	*	*	* /	/ *	*	*	* 1	* 1	* *	*	*	*	*	*	*	*	*	* 1	R 1	•	*	*	*	*	*
Currents																																														
Pier End		*	*	*	* .	/ '	٠,	*	1	*	* 1	*	*	*	*	*	*		*	*	*	*	*	* 1	* *	*	*	* 1	* 1	* *	*	*	*	*	*	*	*	*	* 1	* 1	* *	*	*	*	*	*
Pier Nearshore		*	*	*	*	/	1	*	1	*	* 1	*	*	*	*	*	* 1	A 1	*	*	*	*	*	* 1		*	*	* 1	* 1	* *	*	*	*	*	*	*	*	*	/ 1	* 1		*	*	*	*	*
Beach		/	/	*	*	/	//	′ /	/	*	* 1	* *	*	*	*	*	* 1	* *	*	*	*	*	*	* ,	/ *	*	*	/	/	/ /	•	*	*	*	*	/	/	/	/ '	* ,	-	. /	′ /	/	*	/
Pier End Tide Gege		*	*	*	*	* 1	* 4	*	*	*	* 1	*	*	*	*	*	* '		*	*	1	/	*	* 1		*	*	* 1	* .	/ •	*	*	*	*	/	/	*	*	/ ¹	* •		•	*	/	/	*
Water Characteristi	.CS																																													
Temperature		*	*	*	*	* 1		*	*	*	* 1	*	*	*	*	*	* 1	* 1	*	*	*	*	*	# 1	* #	*	*	* 1	*	* 1		*	*	*	*	*	*	*	* 1	* 1			*	*	*	*
Visibility		*	*	*	*	* 1		*	*	*	* 1	*	*	*	*	*	* 1	* 1	*	*	*	*	*	* 1		*	*	* 1	•	//	*	*	*	*	*	*	*	*	* 1			*	*	*	*	*
Density		*	*	*	*	* 1		*	*	#	* 1	* *	*	*	*	*	* 1	* 1	*	*	*	*	*	* 1		*	*	* 1	*	* *	•	*	*	*	*	/	-	-			- /	*	*	*	*	*
Bathymetric Surveys	1			*								*				*				*				*				*			*	,			*				*	•		,				*
Photography																																														
Beach		*	*	٠	*	* 1		*	*	*	* 1	*	*	*	*	*	* 1	* 1	*	*	-	-	*	# 1	. 4	*	*	* 1	*	* *		*	*	*	*	*	*	/	-	- ,	/ 1			*	*	1
Aerial			*																																			•								

Notes: * Full week of data obtained.

- No data obtained.

8. The annual data summary herein summarizes daily observations by month and year to provide basic data for analysis by users. Daily measurements and observations have already been reported in a series of monthly Preliminary Data Summaries (FRF 1991). If individual data for the present year are needed, the user can obtain detailed information (as well as the monthly and previous annual reports) from the following address:

[/] Less then 7 days of data obtained.

USAE Waterways Experiment Station Coastal Engineering Research Center Field Research Facility 1261 Duck Rd. Kitty Hawk, NC 27949-4472

Although the data collected at the FRF are designed primarily to support ongoing CERC research, use of the data by others is encouraged. Tidal data other than the summaries in this report can be obtained directly from the following address:

National Oceanic and Atmospheric Administration National Ocean Service ATTN: Tide Analysis Branch Rockville, MD 20852

A complete explanation of the exact data desired for specific dates and times will expedite filling any request; an explanation of how the data will be used will help CEIAC or the National Oceanic and Atmospheric Administration (NOAA)/National Ocean Service (NOS) determine whether other relevant data are available. For information regarding the availability of data for all years, contact the FRF at 919-261-3511. Costs for collecting, copying, and mailing will be borne by the requester.

PART II: METEOROLOGY

- 9. This section summarizes the meteorological measurements made during the current year and in combination with all previous years. Meteorological measurements during storms are given in Part IX.
- 10. Mean air temperature, atmospheric pressure, and wind speed and direction were computed for each data file, which consisted of data sampled two times per second for 34 min every 6 hr beginning at or about 0100, 0700, 1300, and 1900 hr eastern standard time (EST); these hours correspond to the time that the National Weather Service (NWS) creates daily synoptic weather maps. During storms, data recordings were made more frequently. Meteorological data are summarized in Table 2.

Table 2
Meteorological Statistics

		Mean	M	ean						Wind Re	sultant	.8
	Air 7	emperature	Atmospi	heric Pres.	P	recipit	ation, i	700		1991	198	0-1991
		deg C		mb	1991		1978-19	91	Speed	Direction	Speed	Direction
<u>Month</u>	1991	1983-1991	1991	1983-1991	Total	Mean	Maxima	Minima	m/sec	deg	m/sec	deg
Jan	7.3	5.9	1018.2	1017.9	142	101	180	44	2.6	341	2.3	333
Feb	7.8	6.8	1015.5	1017.5	8	72	113	20	2.0	306	1.7	342
Mar	11.2	9.7	1009.4	1016.2	186	100	206	35	2.0	268	1.4	355
Apr	15.0	13.7	1015.4	1013.8	73	97	182	0	0.3	322	0.3	328
Macy	22.6	19.2	1015.9	1015.8	7	72	239	20	1.2	156	0.6	187
Jun	26.8	23.8	1013.9	1015.3	59	86	136	27	0.6	92	1.0	198
Jul	29.4	26.4	1012.9	1016.0	150	99	275	19	2.4	217	1.8	210
Aug	26.1	25.9	1014.8	1016.0	114	98	221	30	0.6	159	0.5	97
Sep	25.7	22.8	1017.6	1017.6	7	77	226	5	2.1	63	2.0	40
Oct	21.5	18.2	1016.8	1019.1	124	70	143	17	2.6	15	2.3	26
Nov	16.8	13.6	1018.4	1018.3	46	87	145	26	1.7	321	1.7	344
Dec	9.8	8.1	1019.2	1019.5	97	66	131	4	2.4	294	2.1	328
Average	18.3	16.2	1015.7	1016.9	84	85			0.7	318	0.8	351
Total					1013	1025						

Air Temperature

11. The FRF enjoys a typical marine climate that moderates the temperature extremes of both summer and winter.

Measurement instruments

12. A Yellow Springs Instrument Company, Inc. (YSI) (Yellow Springs, OH) electronic temperature probe with analog output interfaced to the FRF's computer was operated beside the NWS's meteorological instrument shelter located 43 m behind the dune (Figure 2). To ensure proper temperature

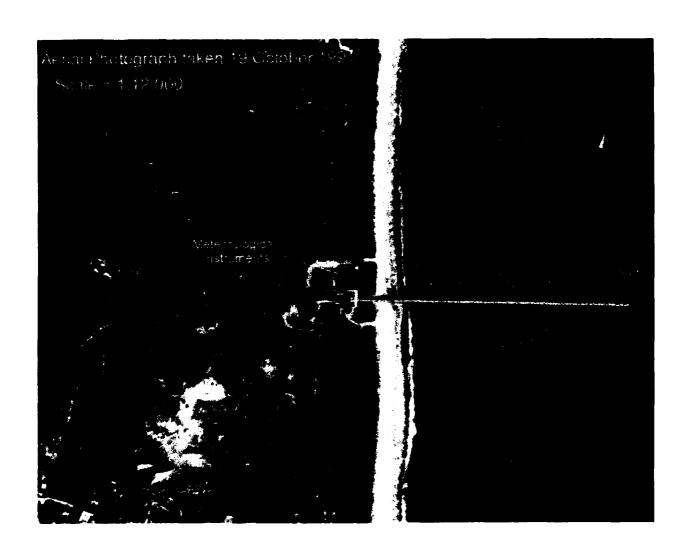


Figure 2. FRF gage locations

readings, the probe was installed 3 m above ground inside a "coolie hat" to shade it from direct sun, yet provide proper ventilation.

Results

13. Daily and average air temperature values are tabulated in Table 2 and shown in Figure 3.

Atmospheric Pressure

Measurement instruments

- 14. <u>Electronic atmospheric pressure sensor</u>. Atmospheric pressure was measured with a YSI electronic sensor with analog output located in the laboratory building at 9 m above NGVD. Data were recorded on the FRF computer. Data from this gage were compared with those from an NWS aneroid barometer to ensure proper operation.
- 15. <u>Microbarograph</u>. A Weathertronics, Incorporated (Sacramento, CA) recording aneroid sensor (microbarograph) located in the laboratory building also was used to continuously record atmospheric pressure variation.
- 16. The microbarograph was compared daily with the NWS aneroid barometer, and adjustments were made as necessary. Maintenance of the microbarograph consisted of inking the pen, changing the chart paper, and winding the clock every 7 days. During the summer, a meteorologist from the NWS checked and verified the operation of the barometer.
- 17. The microbarograph was read and inspected daily using the following procedure:
 - a. The pen was zeroed (where applicable).
 - b. The chart time was checked and corrected, if necessary.
 - c. The daily reading was marked on the chart for reference.
 - <u>d</u>. The starting and ending chart times were recorded, as necessary.
 - e. New charts were installed, when needed.

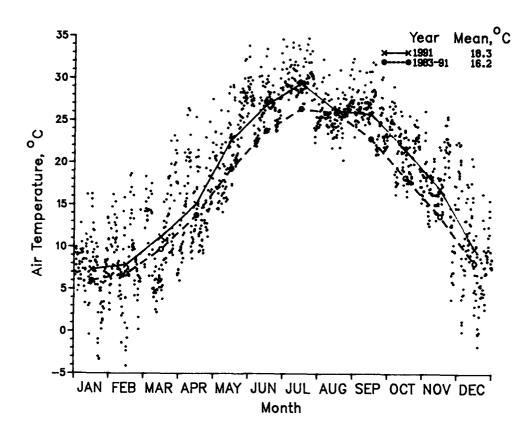


Figure 3. Daily air temperature values with monthly means

Results

18. Daily and average atmospheric pressure values are presented in Figure 4, and summary statistics are presented in Table 2.

Precipitation

19. Precipitation is generally well distributed throughout the year. Precipitation from mid-latitude cyclones (northeasters) predominates in the winter, whereas local convection (thunderstorms) accounts for most of the summer rainfall.

Measurement instruments

20. <u>Electronic rain gage</u>. A Belfort Instrument Company (Baltimore, MD) 30-cm weighing rain gage, located near the instrument shelter 47 m behind the dune, measured daily precipitation. According to the manufacturer, the instrument's accuracy was 0.5 percent for precipitation amounts less than

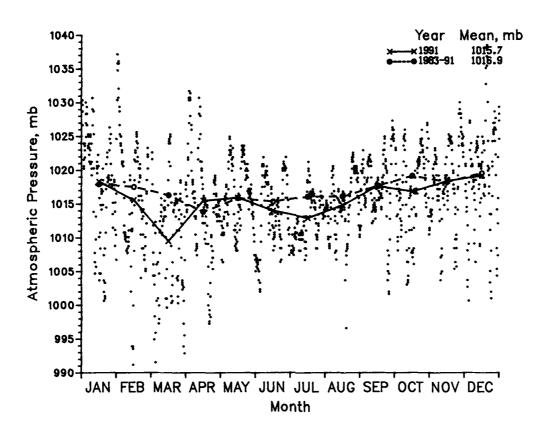


Figure 4. Daily barometric pressure values with monthly means

15 cm and 1.0 percent for amounts greater than 15 cm.

- 21. The rain gage was inspected daily, and the analog chart recorder was maintained by procedures similar to those for the microbarograph.
- 22. <u>Plastic rain gage</u>. An Edwards Manufacturing Company (Alberta Lea, MN) True Check 15-cm-capacity clear plastic rain gage with a 0.025-cm resolution was used to monitor the performance of the weighing rain gage. This gage was located near the weighing gage, and the gages were compared on a daily basis. Very few discrepancies were identified during the year. Results
- 23. Daily and monthly average precipitation values are shown in Figure 5. Statistics of total precipitation for each month during this year and average totals for all years combined are presented in Table 2.

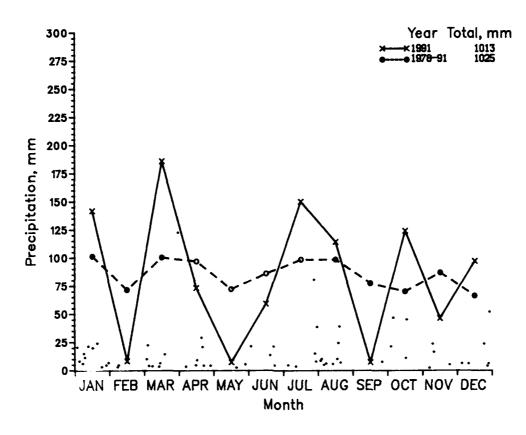


Figure 5. Daily precipitation values with monthly totals

Wind Speed and Direction

24. Winds at the FRF are dominated by tropical maritime air masses that create low to moderate, warm southern breezes; arctic and polar air masses that produce cold winds from northerly directions; and smaller scale cyclonic, low pressure systems, which originate either in the tropics (and move north along the coast) or on land (and move eastward offshore). The dominant wind direction changes with the season, being generally from northern directions in the fall and winter and from southern directions in the spring and summer. It is common for fall and winter storms (northeasters) to produce winds with average speeds in excess of 15 m/sec.

Measurement instrument

25. Winds were measured at the seaward end of the pier at an elevation of 19.1 m (Figure 2) using a Weather Measure Corporation (Sacramento, CA) Skyvane Model W102P anemometer. Wind speed and direction data were collected on the FRF computer. The anemometer manufacturer specifies an accuracy of ±0.45 m/sec below 13 m/sec and 3 percent at speeds above 13 m/sec, with a

threshold of 0.9 m/sec. Wind direction accuracy is ± 2 deg, with a resolution of less than 1 deg. The anemometer is calibrated annually at the National Bureau of Standards in Gaithersburg, MD, and is within the manufacturer's specifications.

Results

26. Annual and monthly joint probability distributions of wind speed versus direction were computed. Wind speeds were resolved into 3-m/sec intervals, whereas the directions were at 22.5-deg intervals (i.e., 16-point compass direction specifications). These distributions are presented as wind "roses," such that the length of the petal represents the frequency of occurrence of wind blowing from the specified direction, and the width of the petal is indicative of the speed. Resultant directions and speeds were also determined by vector-averaging the data (see Table 2). Wind statistics are presented in Figures 6, 7, and 8.

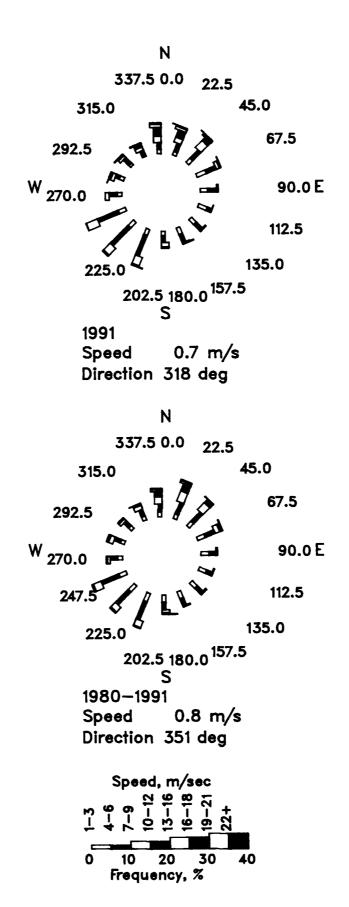


Figure 6. Annual wind roses

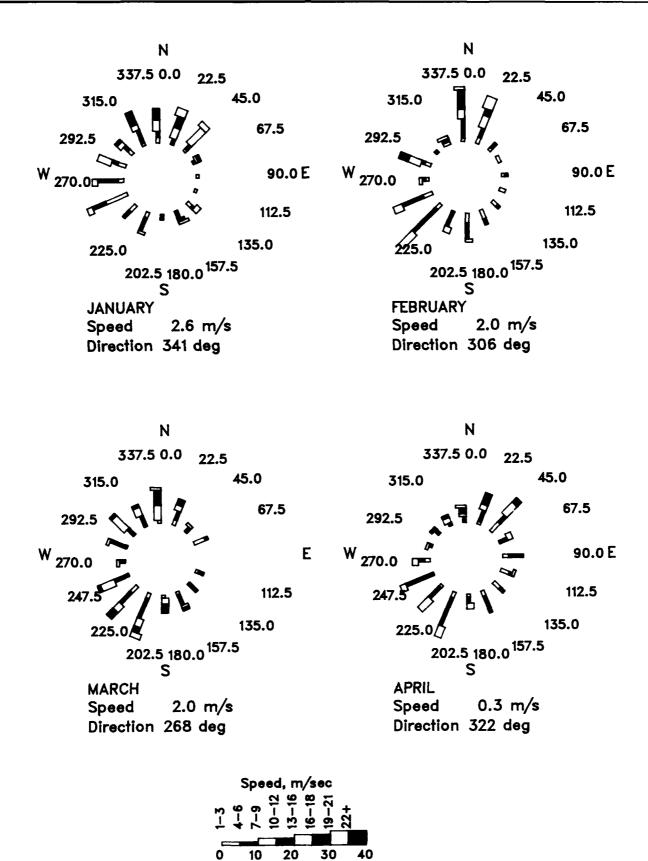
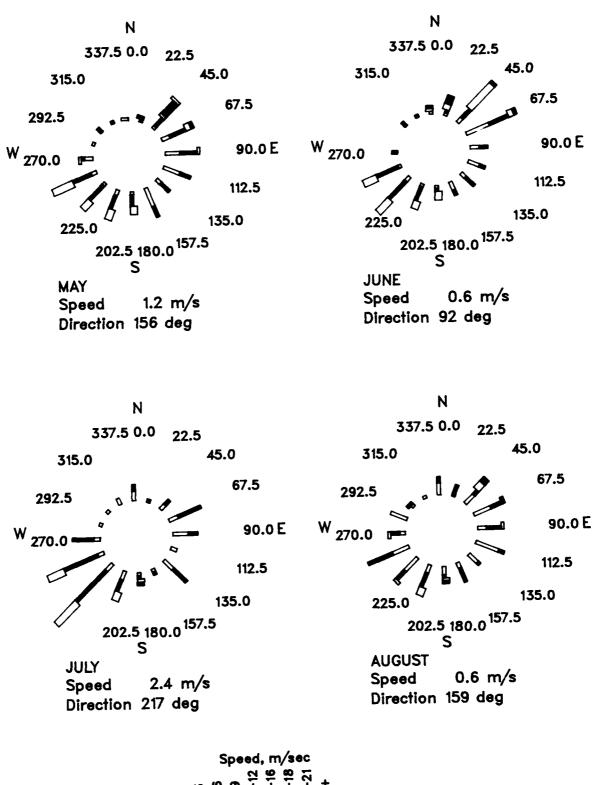


Figure 7. Monthly wind roses for 1991 (Sheet 1 of 3)

Frequency, %



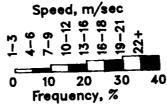
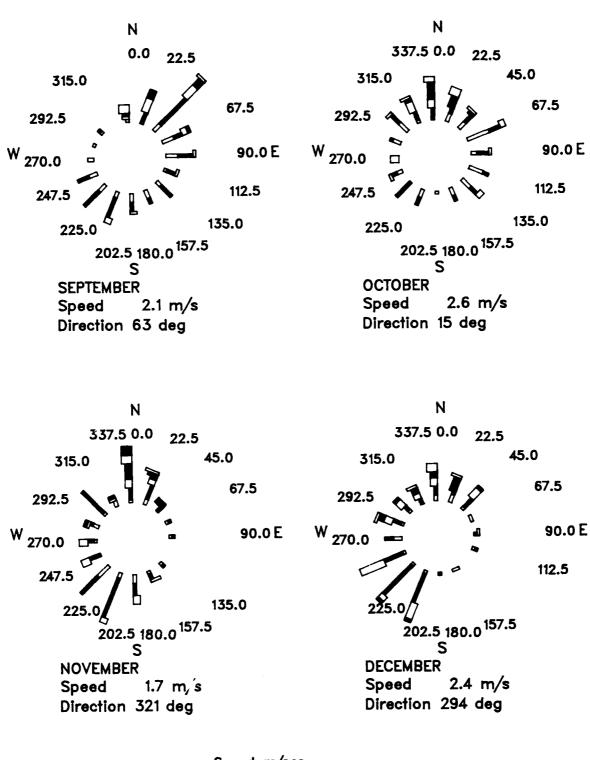


Figure 7. (Sheet 2 of 3)



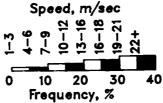


Figure 7. (Sheet 3 of 3)

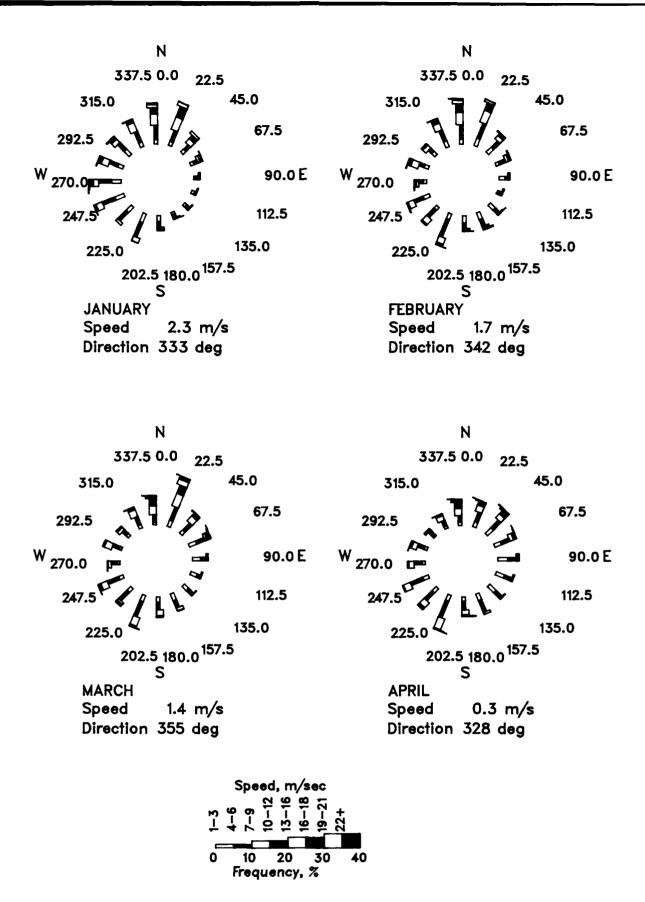


Figure 8. Monthly wind roses for 1980 through 1991 (Sheet 1 of 3)

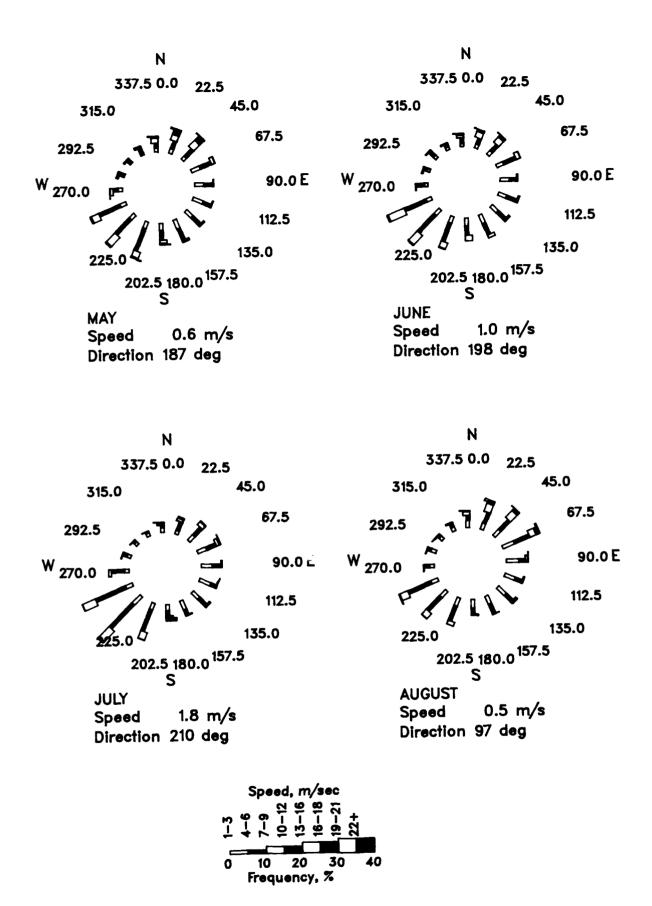
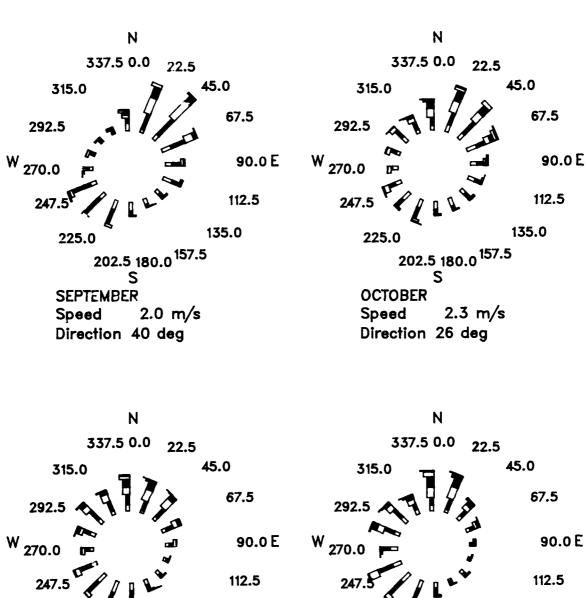
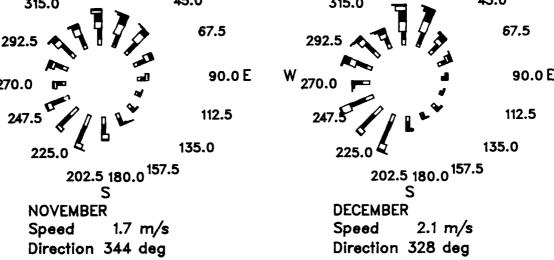


Figure 8. (Sheet 2 of 3)





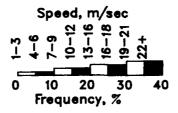


Figure 8. (Sheet 3 of 3)

PART III: WAVES

- 27. This section presents summaries of the wave data. A discussion of individual major storms is given in Part IX and contains additional wave data for times when wave heights exceeded 2 m at the seaward end of the FRF pier. Appendixes B through E provide more extensive data summaries for each gage, including height and period distributions, wave direction distributions, persistence tables, and spectra during storms.
- 28. Wave directions (similar to wind directions) at the FRF are seasonally distributed. Waves approach most frequently from north of the pier in the fall and winter and south of the pier in the summer, with the exception of storm waves that approach twice as frequently from north of the pier.

 Annually, waves are approximately evenly distributed between north and south (resultant wave direction being almost shore-normal).

Measurement Instruments

29. The wave gages included two wave staff gages (Gages 645 and 625), one buoy gage (Gage 630), and one pressure gage (Gage 111) as shown in Figure 2 and located as follows:

	Distance Offshore	Water Depth	Operational
Gage Type/Number	from Baseline	m	Period
Continuous wire (645)	238 m	3.5	11/84-12/91
Continuous wire (625)	567 m	8	11/78-12/91
Accelerometer buoy (630)	6 km	18	11/78-12/91
Pressure gage (111)	1 km	9	09/86-12/91

Staff gages

30. Two Baylor Company (Houston, TX) parallel cable inductance wave gages (Gage 645 at sta 7+80 and Gage 625 at sta 19+00 (Figure 2)) were mounted on the FRF pier. Rugged and reliable, these gages require little maintenance except to keep tension on the cables and to remove any material that may cause an electrical short between them. They were calibrated prior to installation by creating an electrical short between the two cables at known distances along the cable and recording the voltage output. Electronic signal conditioning amplifiers are used to ensure that the output signals from the gages are within a 0- to 5-V range. Manufacturer-stated gage accuracy is about 1.0 percent, with a 0.1-percent full-scale resolution; full scale is 14 m for Gage 625 and 8.2 m for Gage 645. These gages are susceptible to

lightning damage, but protective measures have been taken to minimize such occurrences. A more complete description of the gages' operational characteristics is given by Grogg (1986).

Buoy gage

31. One Datawell Laboratory for Instrumentation (Haarlem, The Netherlands) Waverider buoy gage (Gage 630) measures the vertical acceleration produced by the passage of a wave. The acceleration signal is double-integrated to produce a displacement signal transmitted by radio to an onshore receiver. The manufacturer stated that wave amplitudes are correct to within 3 percent of their actual value for wave frequencies between 0.065 and 0.500 Hz (corresponding to 15- to 2-sec wave periods). The manufacturer also specified that the error gradually increased to 10 percent for wave periods in excess of 20 sec. The results in this report were not corrected for the manufacturer's specified amplitude errors. However, the buoy was calibrated semiannually to ensure that it was within the manufacturer's specification.

Pressure gage

32. One Senso-Metrics, Incorporated (Simi Valley, CA), pressure transduction gage (Gage 111) installed near the ocean bottom measures the pressure changes produced by the passage of waves creating an output signal that is linear and proportional to pressure when operated within its design limits. Predeployment and postdeployment precision calibrations are performed at the FRF using a static deadweight tester. The sensor's range is 0 to 25 psi (equivalent to 0- to 17-m seawater) above atmospheric pressure with a manufacturer-stated accuracy of ± 0.25 percent. Copper scouring pads are installed at the sensor's diaphragm to reduce biological fouling, and the system is periodically cleaned by divers.

Digital Data Analysis and Summarization

- 33. The data were collected, analyzed, and stored on magnetic tape using the FRF's VAX computer. Data sets were normally collected every 6 hr. During storms, the collection was at 3-hr intervals. For each gage, a data set consisted of four contiguous records of 4,096 points recorded at 0.5 Hz (approximately 34 min long), for a total of 2 hr and 16 min. Analysis was performed on individual 34-min records.
 - 34. The analysis program computes the first moment (mean) and the

second moment about the mean (variance) and then edits the data by checking for "jumps," "spikes," and points exceeding the voltage limit of the gage. A jump is defined as a data value greater than five standard deviations from the previous data value, whereas a spike is a data value more than five standard deviations from the mean. If less than five consecutive jumps or spikes are found, the program linearly interpolates between acceptable data and replaces the erroneous data values. The editing stops if the program finds more than five consecutive jumps or spikes, or more than a total of 100 bad points, or the variance of the voltage is below 1×10^{-5} squared volts. The statistics and diagnostics from the analysis are saved.

- 35. Sea surface energy spectra are computed from the edited time series. Spectral estimates are computed from smaller data segments obtained by dividing the 4,096-point record into several 512-point segments. The estimates are then ensemble-averaged to produce a more accurate spectrum. These data segments are overlapped by 50 percent (known as the Welch (1967) method) which has been shown to produce better statistical properties than nonoverlapped segments. The mean and linear trends are removed from each segment prior to spectral analysis. To reduce side-lobe leakage in the spectral estimates, a data window was applied. The first and last 10 percent of data points were multiplied by a cosine bell (Bingham, Godfrey, and Tukey 1967). Spectra were computed from each segment with a discrete Fast Fourier Transform and then ensemble-averaged. Sea surface spectra from subsurface pressure gages were obtained by applying the linear wave theory transfer function.
- 36. Unless otherwise stated, wave height in this report refers to the energy-based parameter H_{mo} defined as four times the zeroth moment wave height of the estimated sea surface spectrum (i.e., four times the square root of the variance) computed from the spectrum passband. Energy computations from the spectra are limited to a passband between 0.05 and 0.50 Hz for surface gages and between 0.05 Hz and a high-frequency cutoff for subsurface gages. This high-frequency limit is imposed to eliminate aliased energy and noise measurements from biasing the computation of H_{mo} and is defined as the frequency where the linear theory transfer function is less than 0.1 (spectral values are multiplied by 100 or more). Smoother and more statistically significant spectral estimates are obtained by band-averaging contiguous spectral components (three components are averaged per band, producing a

frequency band width of 0.0117 Hz).

37. Wave period T_p is defined as the period associated with the maximum energy band in the spectrum, which is computed using a 3-point running average band on the spectrum. The peak period is reported as the reciprocal of the center frequency (i.e., $T_p = 1/\text{frequency}$) of the spectral band with the highest energy. A detailed description of the analysis techniques is presented in a report by Andrews (1987).*

Results

- 38. The wave conditions for the year are shown in Figure 9. For all four gages, the distributions of wave height for the current year and all years combined are presented in Figures 10 and 11, respectively. Distributions of wave period are presented in Figure 12.
- 39. Multiple-year comparisons of data for Gage 111 actually incorporate data for 1985 and 1986 from Gage 640 (a discontinued Waverider buoy previously located at the approximate depth and distance offshore of Gage 111) and data for 1987 from Gage 141, located 30 m south of Gage 111.
- 40. Refraction, bottom friction, and wave breaking contribute to the observed differences in height and period. During the most severe storms when the wave heights exceed 3 m at the seaward end of the pier, the surf zone (wave breaking) has been observed to extend past the end of the pier and occasionally 1 km offshore. This occurrence is a major reason for the differences in the distributions between Gage 630 and the inshore gages. The wave height statistics for the staff gage (Gage 645), located at the landward end of the pier, were considerably lower than those for the other gages. In all but the calmest conditions, this gage is within the breaker zone. Consequently, these statistics represent a lower energy wave climate.
- 41. Summary wave statistics for the current year and all years combined are presented for Gage 630 in Table 3.

^{*} M. E. Andrews. 1987. "Standard Wave Data Anfresis Procedures for Coastal Engineering Applications," unpublished report prepared for the US Army Engineer Waterways Experiment Station, Vicksburg, MS.

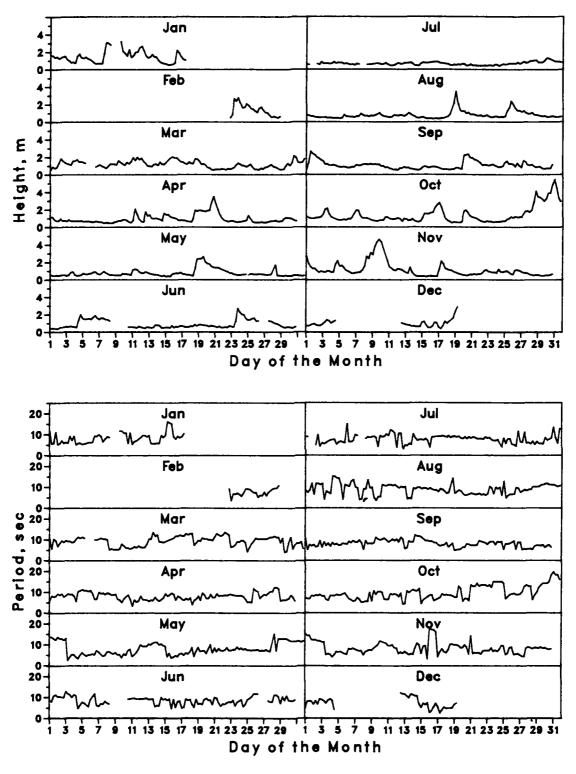


Figure 9. 1991 time histories of wave height and period for Gage 630

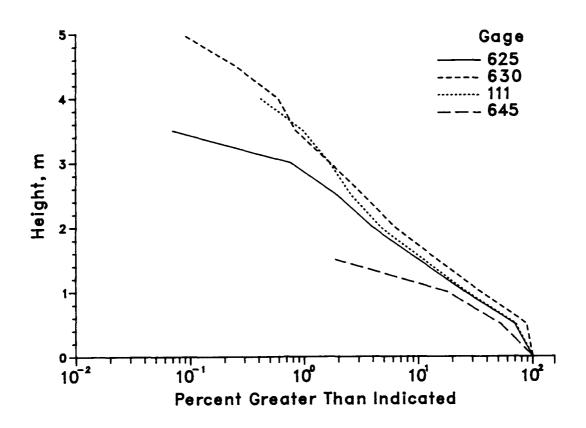


Figure 10. 1991 annual wave height distributions

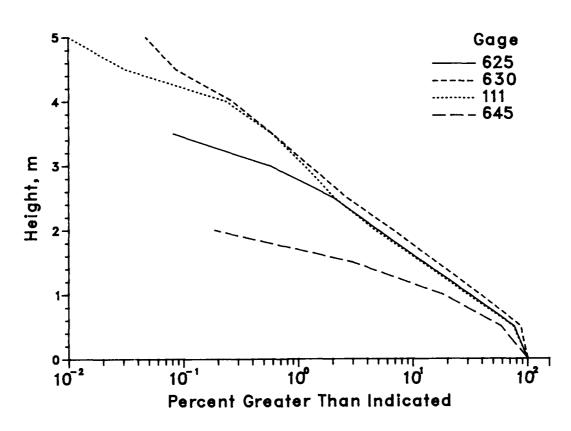


Figure 11. Annual distribution of wave heights for 1980 through 1991

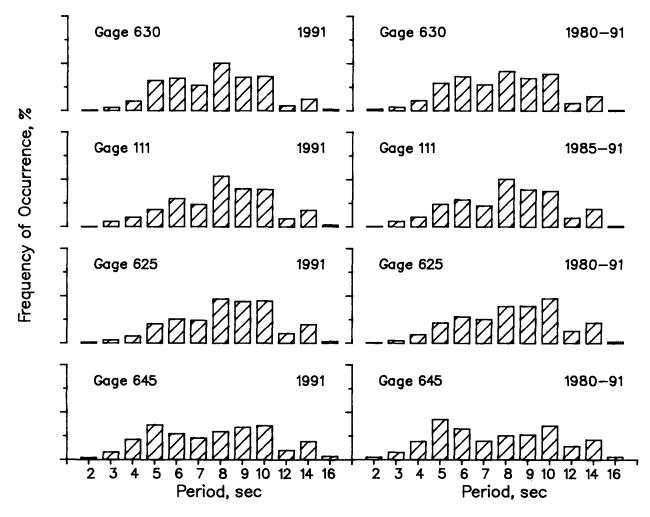


Figure 12. Annual wave period distributions for all gages

Table 3
Wave Statistics for Gage 630

				1991						1	980-1991			
		Hei	ght		Per	Lod			Hei	ght		Per	iod	
		Std.				Std.			Std.				Std.	
	Mean	Dev.	Extreme		Mean	Dev.	Number	Mean	Dev.	Extreme	1	Mean	Dev.	Humber
<u>Month</u>	<u>m</u>	<u>m</u>	<u></u>	Date	50C	Sec	Obs.	<u>m</u>	m_		Date	<u>sec</u>	Sec	Obs.
Jan	1.5	0.7	3.2	9	8.0	2.5	61	1.2	0.7	4.5	1983	8.1	2.7	1255
Feb	1.4	0.7	2.8	23	7.5	1.7	25	1.2	0.7	5.1	1987	8.4	2.6	1146
Mar	1.2	0.5	2.1	30	9.2	2.4	118	1.2	0.7	4.7	1983	8.7	2.6	1358
Apr	1.0	0.6	3.5	20	7.9	1.8	120	1.0	0.6	5.0	1988	8.6	2.6	1327
May	0.8	0.5	2.6	19	7.8	2.9	122	0.9	0.5	3.3	1986	8.1	2.5	1351
Jun	0.9	0.5	2.7	23	8.4	1.9	106	0.8	0.4	2.7	1991	7.8	2.2	1244
Jul	0.7	0.2	1.3	30	7.8	2.1	116	0.7	0.3	2.1	1985	8.1	2.4	1280
Aug	0.8	0.5	3.5	19	8.9	2.5	123	0.8	0.5	3.6	1981	8.2	2.5	1303
Sep	1.1	0.5	2.6	1	8.1	1.7	119	1.1	0.6	6.1	1985	8.6	2.6	1310
Oct	1.4	1.0	5.4	31	9.7	3.4	122	1.3	0.7	5.4	1991	8.8	2.8	1361
Nov	1.1	0.9	4.6	9	8.2	2.9	118	1.1	0.7	4.6	1991	7.9	2.8	1155
Dec	1.0	0.5	2.9	19	7.5	2.6	41	1.2	0.8	5.6	1980	8.2	2.9	1108
Annual	1.1	0.6	5.4	Oct	8.3	2.6	1191	1.0	0.6	6.1	Sep 1985	8.3	2.6	15198

- 42. Annual joint distributions of wave height versus wave period for Gage 630 are presented for 1991 in Table 4, and for all years combined in Table 5. Similar distributions for the other gages are included in Appendixes B-E.
- 43. Annual distributions of wave directions (relative to true north) based on daily observations of direction at the seaward end of the pier and height from Gage 625 (or Gage 111 when data for Gage 625 were unavailable) are shown in Figure 13. Monthly wave "roses" for 1991 and all years combined are presented in Figures 14 and 15, respectively.

Table 4 $Annual \ (1991) \ Joint \ Distribution \ of \ H_{mo} \ \ versus \ T_p \ \ for \ Gage \ 630*$

		_				1	eriod,	sec					
	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-	
Height, m	<u>2,9</u>	<u>3,9</u>	4,9	<u>5.9</u>	<u>6,9</u>	7.9	<u>8.9</u>	9,9	<u>11.9</u>	<u>13.9</u>	<u> 15.9</u>	Longer	Total
0.00 - 0.49	8	17	17	50	50	84	319	243	168	34	126	25	1141
0.50 - 0.99	17	118	285	596	655	579	982	840	974	101	218		5365
1.00 - 1.49			84	437	269	193	537	218	176	25	92		2031
1.50 - 1.99			17	176	227	101	92	76	101	17	34		841
2.00 - 2.49				25	118	50	42	25	25	8			293
2.50 - 2.99					50	50	34			8	17		159
3.00 - 3.49					8	25		8	8	17	8	8	82
3.50 - 3.99							8			8	8		24
4.00 - 4.49							8	8	8			8	32
4.50 - 4.99								8				8	16
5.00 - Greater												8	8
Total	25	135	403	1284	1377	1082	2022	1426	1460	218	503	57	

^{*} Percent occurrence (x100) of height and period.

						P	eriod.	Sec				-	_
Height, m											14.0- _15.9	16.0- Longer	<u>Total</u>
0.00 - 0.49	27	14	26	60	86	114	332	278	189	66	126	5	1323
0.50 - 0.99	37	136	255	509	592	526	882	744	801	140	229	16	4867
1.00 - 1.49		.9	143	405	424	251	284	212	322	40	121	3	2214
1.50 - 1.99			13	164	245	111	83	78	126	32	72	4	928
2.00 - 2.49			1	24	95	67	54	37	59	27	36	1	401
2.50 - 2.99				1	12	32	18	13	32	10	24	1	143
3.00 - 3.49					1	12	12	12	14	5	8	1	65
3.50 - 3.99						1	6	7	11	4	5	•	34
4.00 - 4.49							2	4	7	1	3	1	18
4.50 - 4.99								1	2			1	4
5.00 - Greater							1		1	1	1	1	5
Total	64	159	438	1163	1455	1114	1674	1386	1564	326	625	34	_

^{*} Percent occurrence (x100) of height and period.

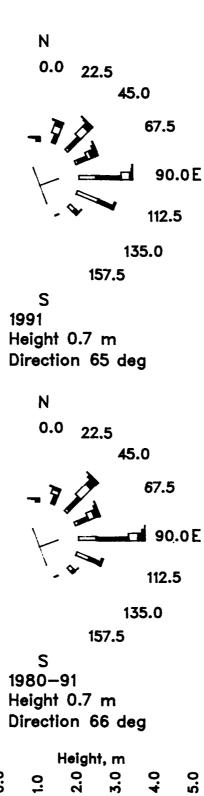
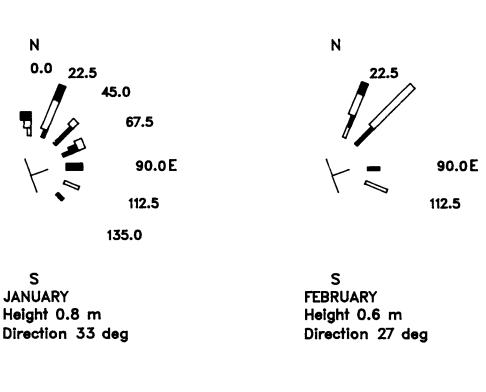
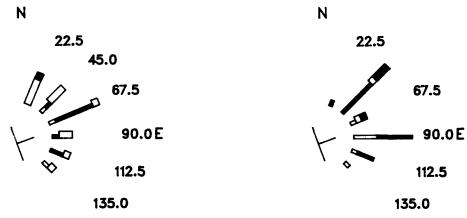


Figure 13. Annual wave roses







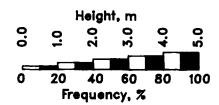
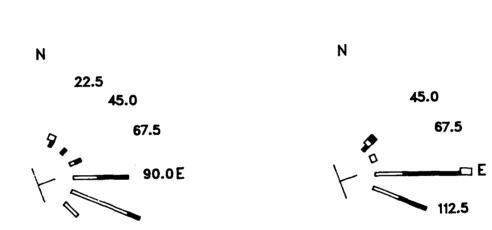


Figure 14. Monthly wave roses for 1991 (Sheet 1 of 3)





135.0

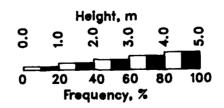
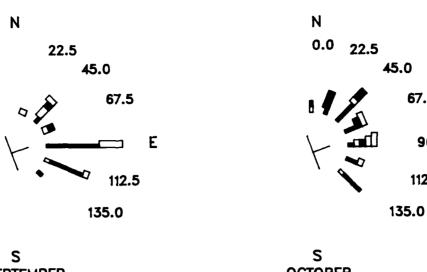


Figure 14. (Sheet 2 of 3)

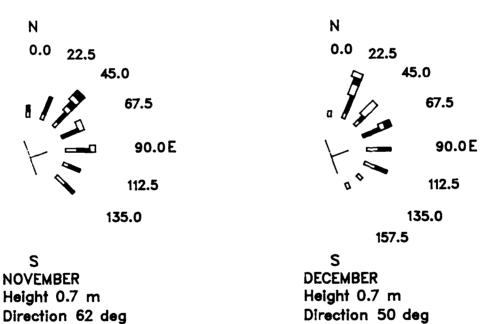


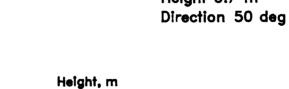
67.5

90.0E

112.5

OCTOBER SEPTEMBER Height 1.0 m Height 0.9 m Direction 68 deg Direction 78 deg



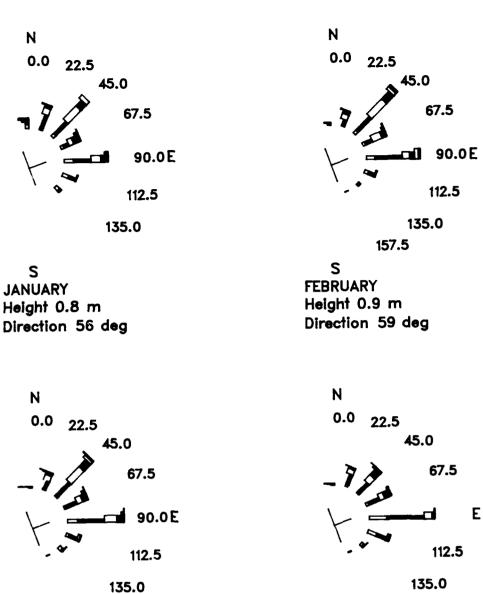


100

Figure 14. (Sheet 3 of 3)

Frequency, %

40 60



S MARCH Height 0.9 m Direction 63 deg

157.5

157.5 S APRIL Height 0.8 m Direction 67 deg

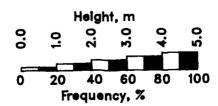
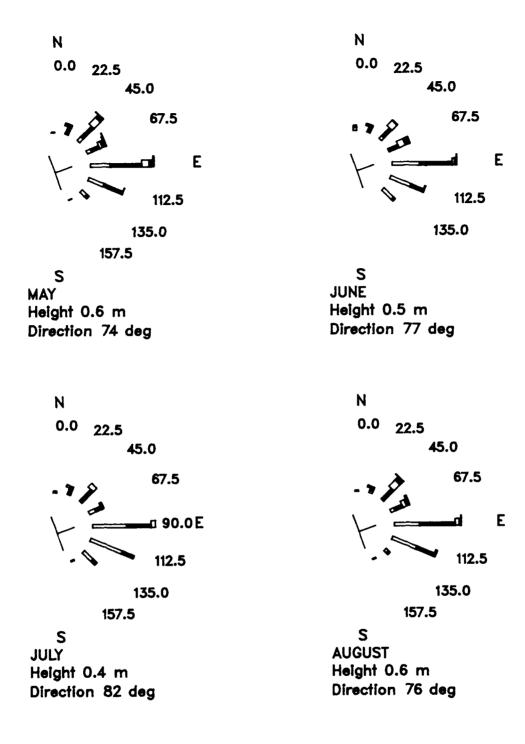


Figure 15. Monthly wave roses for 1980 through 1991 (Sheet 1 of 3)



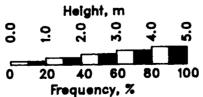
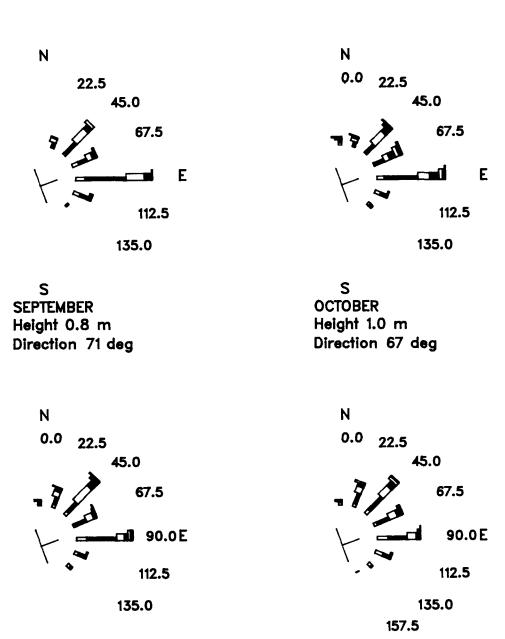
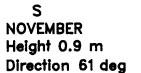


Figure 15. (Sheet 2 of 3)





S DECEMBER Height 0.8 m Direction 58 deg

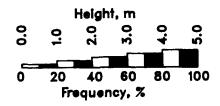


Figure 15 (Sheet 3 of 3)

PART IV: CURRENTS

44. Surface current speed and direction at the FRF are influenced by winds, waves, and, indirectly, by the bottom topography. The extent of the respective influences varies daily. However, winds tend to dominate the currents at the seaward end of the pier, whereas waves dominate within the surf zone.

Observations

45. Near 0700 EST, daily observations of surface current speed and direction were made at (a) the seaward end of the pier, (b) the midsurf position on the pier, and (c) 10 to 15 m from the beach 500 m updrift of the pier. Surface currents were determined by observing the movement of dye on the water surface.

Results

46. Annual mean and mean currents for 1980 through 1991 are presented in Table 6 and in Figure 16. Figure 16 shows the daily and average annual measurements at the beach, pier midsurf, and pier end locations. Since the relative influences of the winds and waves vary with position from shore, the current speeds and, to some extent, direction vary at the beach, midsurf, and pier end locations. Magnitudes generally are largest at the midsurf location and lowest at the end of the pier.

Table 6

Mean Longshore Surface Currents*

	Pier End, cm/sec		Pier Midsu	rf. cm/sec	Beach, cm/sec	
		1980-		1980-		1980-
Month	<u>1991</u>	<u> 1991</u>	<u>1991</u>	1991	<u>1991</u>	1991
Jan	30	22	20	18	1	5
Feb	-6	5	1	5	5	8
Mar	11	14	5	8	3	8
Apr	15	13	23	12	-2	2
May	28	19	15	5	10	4
Jun	17	11	14	3	16	5
Jul	0	2	2	-7	-4	-8
Aug	20	15	7	-2	1	-2
Sep	7	7	11	1	-1	-2
Oct	-5	1	-7	-4	-10	-5
Nov	-3	5	-1	4	-4	4
Dec	11	13	9	13	-1	5
Annual	10	11	8	5	1	2

^{* + =} southward; - = northward.

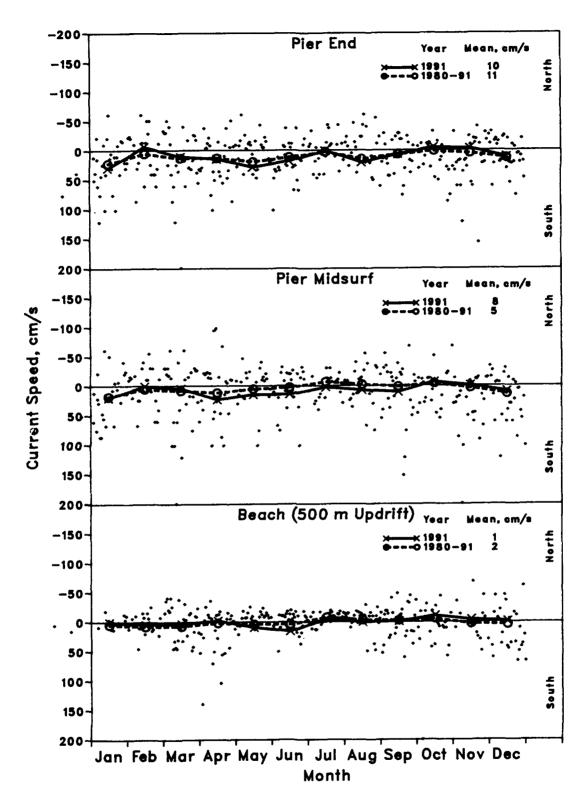


Figure 16. Daily current speeds and directions with monthly means for 1991

PART V: TIDES AND WATER LEVELS

Measurement Instrument

- 47. Water level data were obtained from an NOAA/NOS control tide station (sta 865-1370) located at the seaward end of the research pier (Figure 2) by using a Leupold and Stevens, Inc. (Beaverton, OR) digital tide gage. This analog-to-digital recorder is a float-activated, negator-spring, counterpoised instrument that mechanically converts the vertical motion of a float into a coded, punched paper tape record. The below-deck installation at pier sta 19+60 consisted of a 30.5-cm-diam stilling well with a 2.5-cm orifice and a 21.6-cm-diam float.
- 48. Operation and tending of the tide gage conformed to NOS standards. The gage was checked daily for proper operation of the punch mechanism and for accuracy of the time and water level information. The accuracy was determined by comparing the gage level reading with a level read from a reference electric tape gage. Once a week, a heavy metal rod was lowered down the stilling well and through the orifice to ensure free flow of water into the well. During the summer months, when biological growth was most severe, divers inspected and cleaned the orifice opening as required.
- 49. The tide station was inspected quarterly by an NOAA/NOS tide field group. Tide gage elevation was checked using existing NOS control positions, and the equipment was checked and adjusted as needed. Both NOS and FRF personnel also reviewed procedures for tending the gage and handling the data. Any specific comments on the previous months of data were discussed to ensure data accuracy.
- 50. Digital paper tape records of tide heights taken every 6 min were analyzed by the Tides Analysis Branch of NOS. An interpreter created a digital magnetic computer tape from the punch paper tape, which was then processed on a large computer. First, a listing of the instantaneous tidal height values was created for visual inspection. If errors were encountered, a computer program was used to fill in or recreate bad or missing data using correct values from the nearest NOS tide station and accounting for known time lags and elevation anomalies. The data were plotted, and a new listing was generated and rechecked. When the validity of the data had been confirmed, monthly tabulations of daily highs and lows, hourly heights (instantaneous

height selected on the hour), and various extreme and/or mean water level statistics were computed.

Results

51. Tides at the FRF are semidiurnal with both daily high and low tides approximately equal. Tide height statistics are presented in Table 7. Figure 17 plots the monthly tide statistics for all available data, and Figure 18 compares the distribution of daily high and low water levels and hourly tide heights. The monthly or annual mean sea level (MSL) reported is the average of the hourly heights, whereas the mean tide level is midway between mean high water (MHW) and mean low water (MLW), which are the averages of the daily high— and low—water levels, respectively, relative to NGVD. Mean range (MR) is the difference between MHW and MLW levels, and the lowest water level for the month is the extreme low (EL) water, while the highest water level is the extreme high (EH) water level.

Table 7

<u>Tide Height Statistics*</u>

Month	Mean	Mean	Mean	Mean					
OL	High	Tide	Sea	Low	Mean	Extreme		Extreme	
Year	Water	<u>Level</u>	Level	<u>Water</u>	Range	<u>High</u>	<u>Date</u>	Low	Date
					<u>1991</u>				
Jan	55	13	14	-28	83	87	2	~55	1
Feb	47	7	7	-33	80	85	26	~77	17
Mar	58	17	17	-24	82	88	30	~58	1
Apr	52	12	12	-28	80	101	21	~52	13
May	51	11	11	-29	80	92	18	~50	13
Jun	59	19	19	-22	81	106	23	~55	12
Jul	58	17	18	-23	81	88	11	~54	43
Aug	55	15	15	-26	81	82	25	~52	10
Sep	59	18	18	-23	82	95	1	~46	30
Oct	65	24	25	-16	81	125	31	~40	9
Nov	60	19	19	-21	81	118	1	~58	20
Dec	46	5	6	-35	81	96	24	~83	21
1991	55	15	15	-26	81	125	Oct	-83	Dec
				1	rior Year	<u>:\$</u>			
1990	49	9	9	-32	81	109	May	~78	Feb
1989	49	9	9	-31	80	199	Mar	-77	Apr
1988	46	6	7	-33	79	129	Apr	-72	Dec
1987	55	15	16	-24	79	113	Jan	-63	Nov
1986	60	13	13	-35	95	123	Dec	-108	Jan
1985	59	10	11	-37	96	136	Dec	-93	Apr
1984	64	16	16	-32	97	147	Oct	-77	Jul
1983	68	19	19	-30	98	143	Jan	-73	Mar
1982	58	8	9	-42	99	127	Oct	-108	Feb
1981	59	8	9	-42	101	149	Nov	-110	Apr
1980	59	8	8	-43	102	118	Mar	-119	Mar
1979	60	9	9	-43	103	121	Feb	-95	Sep
1979-									
1991	57	11	11	-35	93	199	Mar 1989	-119	Mar 198

^{*} Measurements are in centimeters.

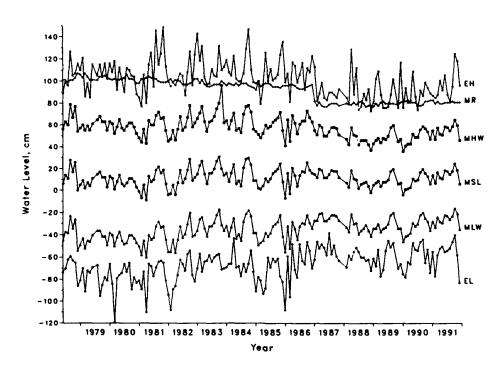


Figure 17. Monthly tide and water level statistics relative to NGVD

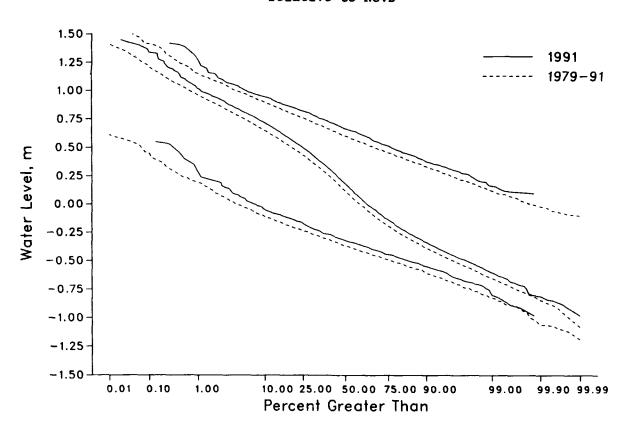


Figure 18. Distributions of hourly tide heights and high— and low-water levels

PART VI: WATER CHARACTERISTICS

52. Monthly averages of daily measurements of surface water temperature, visibility, and density at the seaward end of the FRF pier are given in Table 8. The summaries represent single observations made near 0700 EST and, therefore, may not reflect daily average conditions since such characteristics can change within a 24-hr period. Large temperature variations were common when there were large differences between the air and water temperatures and variations in wind direction. From past experience, persistent onshore winds move warmer surface water toward the shoreline, although offshore winds cause colder bottom water to circulate shoreward, resulting in lower temperatures.

Table 8

Mean Surface Water Characteristics

	•	rature g C	Visib	ility	Dens 	
		1980-		1980-		1980-
Month	<u>1991</u>	<u>1991</u>	<u>1991</u>	1991	<u> 1991</u>	1991
Jan	8.9	6.1	1.6	1.3	1.0223	1.023
Feb	9.1	5.6	2.2	1.8	1.0228	1.023
Mar	10.1	7.1	1.7	1.6	1.0225	1.022
Apr	12.5	11.1	2.5	2.3	1.0219	1.022
May	17.6	15.5	2.5	2.4	1.0211	1.022
Jun	22.4	19.6	2.6	3.4	1.0202	1.021
Jul	23.6	22.1	4.8	3.8	1.0213	1.021
Aug	25.1	23.9	2.7	3.2	1.0206	1.020
Sep	23.9	23.1	2.7	2.3	1.0212	1.020
Oct	20.2	19.5	1.8	1.6	1.0218	1.021
Nov	13.9	14.8	1.2	1.1	1.0237	1.022
Dec	11.7	10.1	1.3	1.1	1.0248	1.023
Annual	16.6	14.9	2.3	2.1	1.0220	1.022

Temperature

53. Daily sea surface water temperatures (Figure 19) were measured with an NOS water sampler and thermometer. Monthly mean water temperatures (Table 8) varied with the air temperatures (see Table 2).

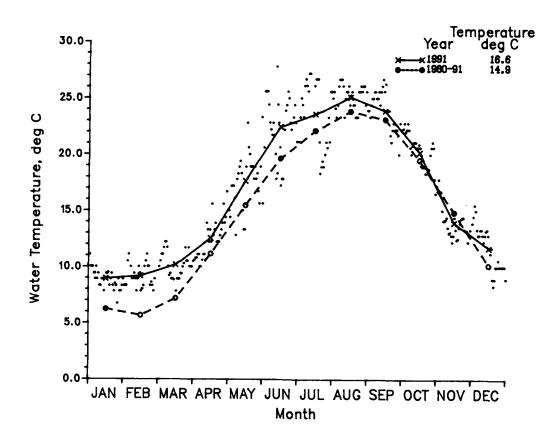


Figure 19. Daily water temperature values with monthly means

Visibility

- 54. Visibility in coastal nearshore waters depends on the amount of salts, soluble organic material, detritus, living organisms, and inorganic particles in the water. These dissolved and suspended materials change the absorption and attenuation characteristics of the water that vary daily and yearly.
- 55. Visibility was measured with a 0.3-m-diam Secchi disk, and similar to water temperature, variation was related to onshore and offshore winds. Onshore winds moved warm clear surface water toward shore, whereas offshore winds brought up colder bottom water with large concentrations of suspended matter. Figure 20 presents the daily and monthly mean surface visibility values for the year. Large variations were common, and visibility less than 1 m was expected in any month. Monthly means are given in Table 8.

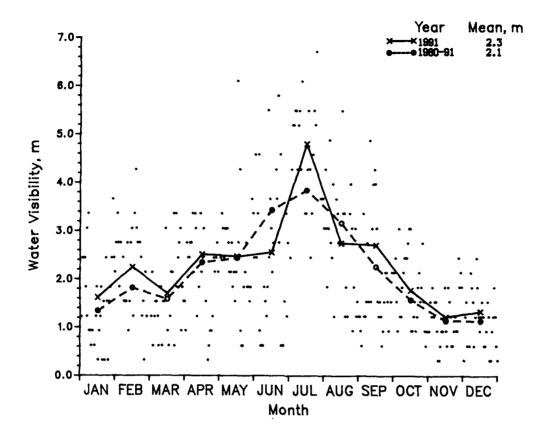


Figure 20. Daily water visibility values with monthly means

Density

56. Daily and monthly mean surface density values, plotted in Figure 21, were measured with a hydrometer. Monthly means are also given in Table 8.

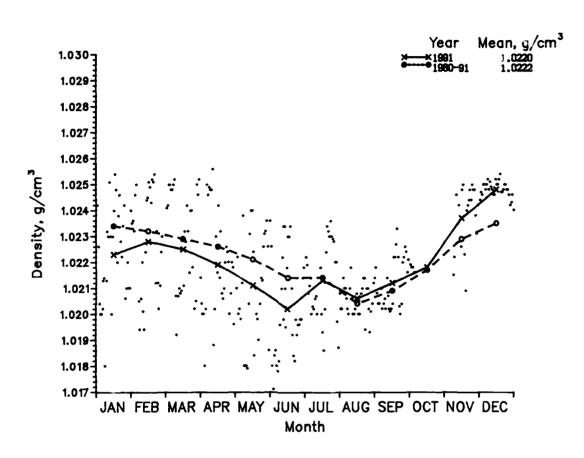


Figure 21. Daily water density values with monthly means

PART VII: SURVEYS

- 57. Waves and currents interacting with bottom sediments produce changes in the beach and nearshore bathymetry. These changes can occur very rapidly in response to storms, or slowly as a result of persistent but less forceful seasonal variations in wave and current conditions.
- 58. Nearshore bathymetry at the FRF is characterized by regular shore-parallel contours, a moderate slope, and a barred surf zone (usually an outer storm bar in water depths of about 4.5 m and an inner bar in water depths between 1.0 and 2.0 m). This pattern is interrupted in the immediate vicinity of the pier where a permanent trough runs under much of the pier, ending in a scour hole where depths can be up to 3.0 m greater than the adjacent bottom (Figure 22). This trough, which apparently is the result of the interaction of waves and currents with the pilings, varies in shape and depth with changing wave and current conditions. The effect of the pier on shore-parallel contours occurs as far as 300 m away, and the shoreline may be affected up to 350 m from the pier (Miller, Birkemeier, and DeWall 1983).

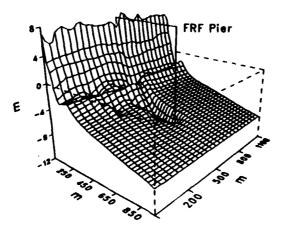


Figure 22. Permanent trough under the FRF pier, 23 September 1991

- 59. Approximately once a month, surveys were conducted of an area extending 600 m north and south of the pier and approximately 950 m offshore. This was done in order to document the temporal and spatial variability in bathymetry. Contour maps resulting from these surveys, along with plots of change in elevation between surveys, are given in Appendix A.
- 60. All surveys used the Coastal Research Amphibious Buggy (CRAB), a 10.7-m-tall amphibious tripod described by Birkemeier and Mason (1984), and a Geodimeter electronic surveying system, a Geodimeter 140-T self-tracking, electronic theodolite, distance meter. The profile locations are shown in each figure in Appendix A. Monthly soundings along both sides of the FRF pier were collected by lowering a weighted measuring tape to the bottom and recording the distance below the pier deck. Soundings were taken midway between the pier pilings to minimize errors caused by scour near the pilings.
- 61. A history of bottom elevations below Gages 645 and 625 is presented in Figure 23 for pier stations 7+80 (238 m) and 18+60 (567 m), along with intermediate locations, 323 and 433 m.

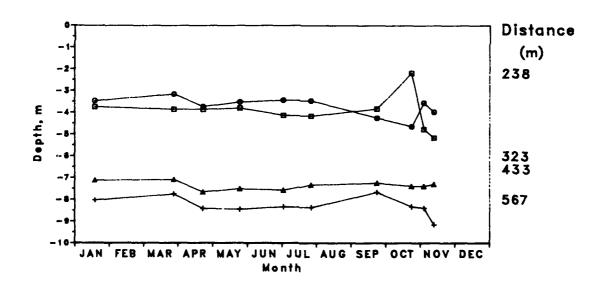


Figure 23. Time history of bottom elevations at selected locations under the FRF pier

PART VIII: PHOTOGRAPHY

Aerial Photographs

62. Aerial photographs were taken biannually using a 23-cm aerial mapping camera at a scale of 1:12,000. All coverage was at least 60-percent overlap, with flights flown as closely as possible to low tide between 1000 and 1400 EST with less than 10-percent cloud cover. The flight lines covered are shown in Figure 24. Figure 25 is a sample of the imagery obtained on 23 January 1990; the available aerial photographs for the year are:

<u>Date</u>	Flight Lines	<u>Format</u>
14 Jan	1	B/W
	2	Color

Beach Photographs

63. Daily color slides of the beach were taken using a 35-mm camera from the same location on the pier looking north and south (Figure 26). The location from which each picture was taken, as well as the date, time, and a brief description of the picture, were marked on each of the slides.

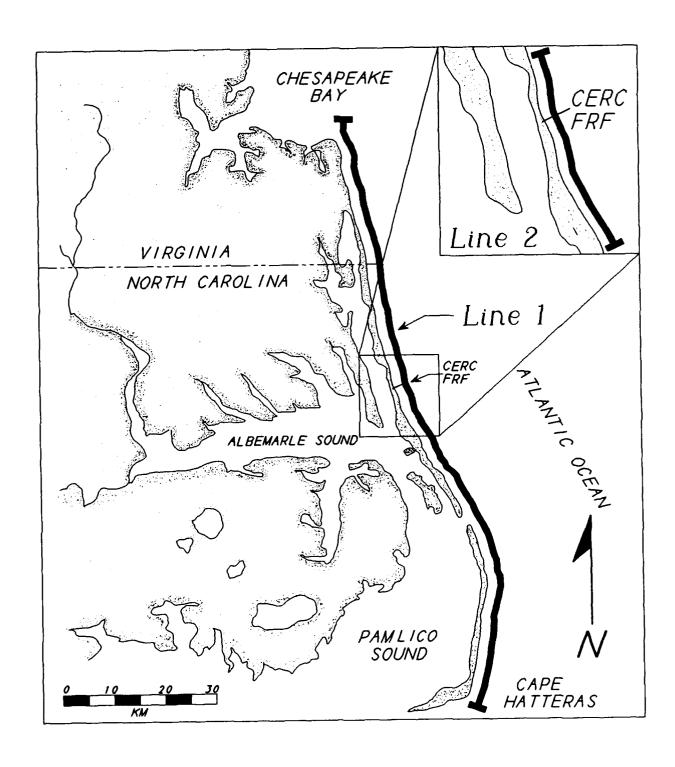
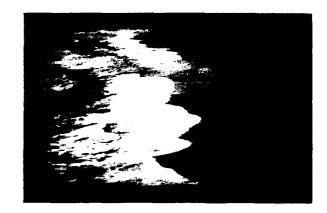


Figure 24. Aerial photography flight lines



Figure 25. Sample aerial photograph, 23 January 1990 (Scale = 1:12,000)





a. 10 January 1991





b. 10 February 1991

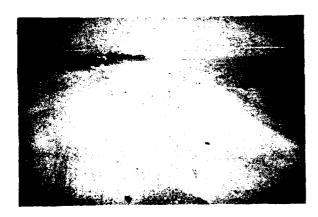




c. 10 March 1991

Figure 26. Beach photos looking north and south from the FRF pier (Sheet 1 of 4)

South View





d. 10 April 1991





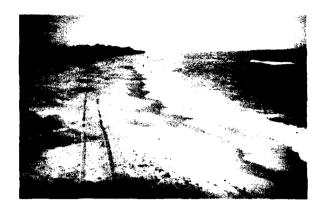
e. 10 May 1991

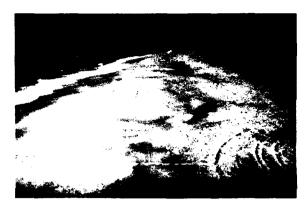




f. 5 June 1991

Figure 26. (Sheet 2 of 4)





g. 10 July 1991





h. 10 August 1991



i. 10 September 1991

Figure 26. (Sheet 3 of 4)





j. 10 October 1991





k. 11 November 1991





1. 8 December 1991
Figure 26. (Sheet 4 of 4)

PART IX: STORMS

64. This section discusses storms (defined here as times when the wave height parameter, H_{mo} , equaled or exceeded 2 m at the seaward end of the FRF pier). Sample spectra from Gage 630 are given in Appendix B. Prestorm and/or poststorm bathymetry diagrams are given in Appendix A. Tracking information was provided by NOAA Daily Weather Maps (US Department of Commerce 1991).

7-9 January 1991 (Figure 27)

65. Winds from a strong Canadian high-pressure system began to generate storm waves at the FRF late on 7 January. Development of a weak coastal storm off the Georgia coast early on 8 January prolonged the period of onshore winds. The maximum $H_{\rm so}$ (at Gage 625) of 2.96 m ($T_{\rm p}$ = 10.67 sec) was attained at 2342 EST on 8 January. Maximum winds (from the northeast) approaching 15 m/s occurred at 2042 EST on 7 January.

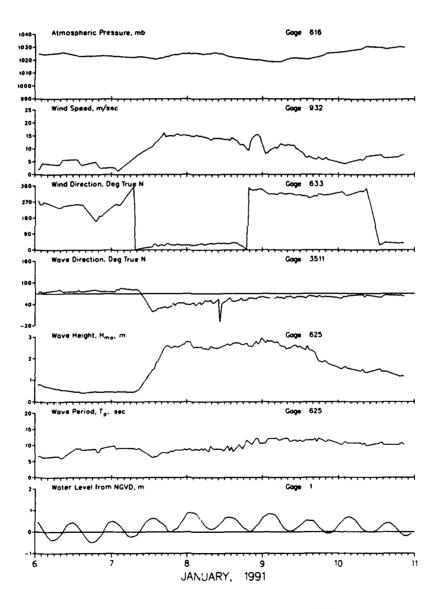


Figure 27. Data for 7-9 January 1991 storm

11-12 January 1991 (Figure 28)

66. Following directly behind the storm on 8 January, another Canadian high-pressure system briefly regenerated storm waves at the FRF. Maximum winds (from the southeast) exceeding 13 m/s peaked at 2042 EST on 11 January with the maximum H_{mo} (at Gage 625) of 2.25 m (T_p = 8.83 sec) occurring early the next day at 0100 EST.

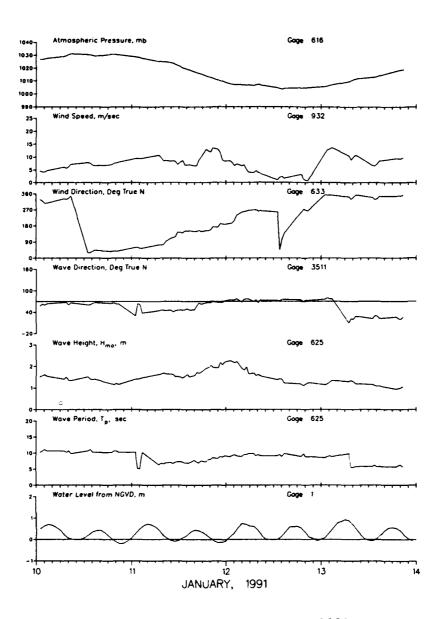


Figure 28. Data for 11-12 January 1991 storm

23 February 1991 (Figure 29)

67. Developing in the Gulf of Mexico off Texas on 20 February, this weak storm slowly moved across the southern U.S., being located over South Carolina on 23 February and moving offshore the following day. Peak winds (from the north-northeast) approached 16 m/s at 0508 EST on 23 February. The maximum H_{mo} (at Gage 625), which was recorded later that day at 1900 EST, reached 2.30 m (T_{p} = 7.53 sec). The minimum atmospheric pressure of 1,003.4 mb occurred at 1708 EST on 22 February. There was no precipitation at the FRF from this storm.

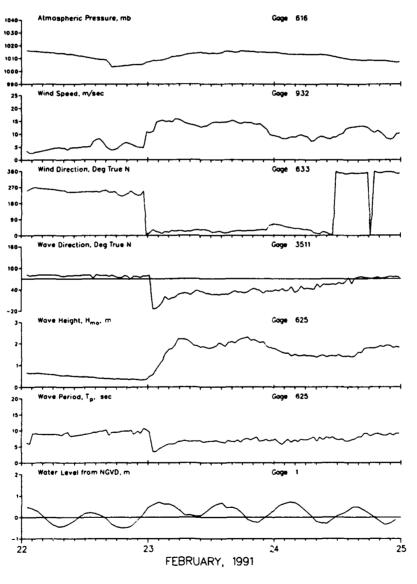


Figure 29. Data for 23 February 1991 storm

6-7 March 1991 (Figure 30)

68. Winds from a strong Canadian high-pressure system began to generate storm waves at the FRF late on 6 March. The maximum $H_{\rm mo}$ (at Gage 625) of 2.50 m ($T_{\rm p}$ = 7.53 sec) was attained at 0208 EST on 7 March. Maximum winds (from the northeast) exceeding 16 m/s occurred at 0542 EST also on 7 March.

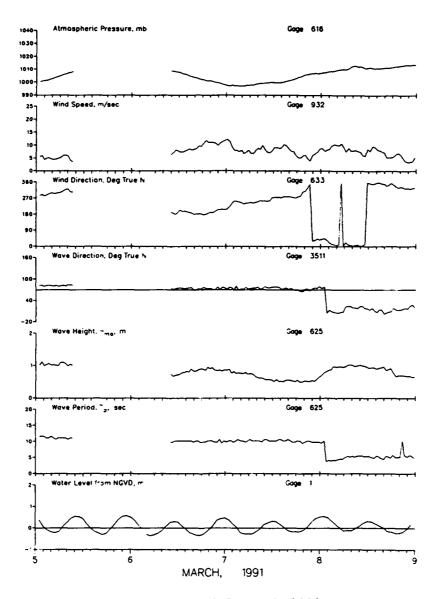


Figure 30. Data for 6-7 March 1991 storm

29 March 1991 (Figure 31)

69. Developing over South Carolina on 29 March, this storm rapidly moved to the northeast, being located off the Virginia coast by 30 March. Maximum winds approaching 16 m/s peaked at 1634 EST on 29 March with the maximum H_{mo} (at Gage 625) of 2.22 m ($T_{\rm p}$ = 6.92 sec) occurring later the same day at 1934 EST. The minimum atmospheric pressure of 1,014.0 mb was recorded at 0400 EST on 30 March. Total precipitation was 30 mm.

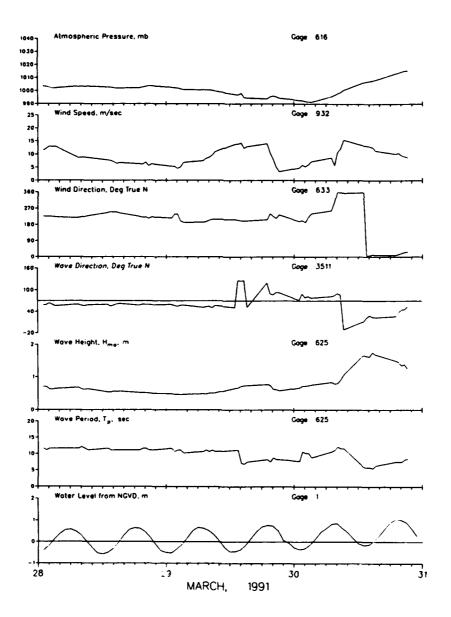


Figure 31. Data for 29 March 1991 storm

20-21 April 1991 (Figure 32)

70. Developing off Cape Hatteras, NC on 20 April, this intense coastal storm quickly deepened and moved up the coast, being located off the Maryland coast early on 21 April and over Canada by 22 April. Maximum wind speeds near 17 m/s (from the north-northeast) were recorded at 1600 EST on 20 April, with the maximum $H_{\rm mo}$ (at Gage 625) of 2.81 m ($T_{\rm p}$ = 8.83 sec) occurring several hours later at 2020 EST. This was followed the next morning at 0208 EST by the minimum atmospheric pressure of 998.4 mb. Total precipitation at the FRF from this system was 42 mm.

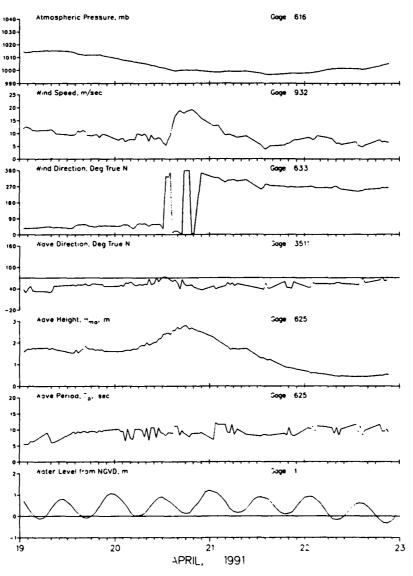


Figure 32. Data for 20-21 April 1991 storm

18-19 May 1991 (Figure 33)

71. Winds from a strong Canadian high-pressure system began to generate storm waves at the FRF late on 18 May. The maximum $H_{\rm mo}$ (at Gage 625) of 2.43 m ($T_{\rm p}$ = 6.92 sec) was attained at 1000 EST on 19 May. Maximum winds (from the northeast) neared 14 m/s at 0842 EST, also on 19 May.

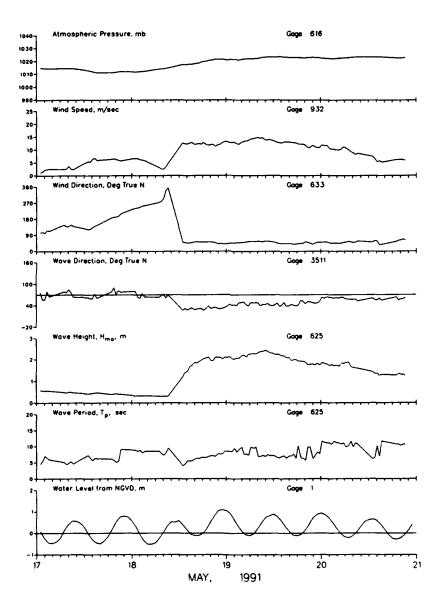


Figure 33. Data for 18-19 May 1991 storm

23 June 1991 (Figure 34)

72. Development of a weak coastal storm off the North Carolina coast early on 22 June produced a short period of storm waves. The maximum $H_{\rm mo}$ (at Gage 625) of 2.43 m ($T_{\rm p}$ = 8.26 sec) was attained at 2042 EST on 23 June. This coincided with the maximum winds (from the north-northeast) which exceeded 14 m/s and occurred at 2008 EST. The minimum atmospheric pressure of 1,006.3 mb was recorded on 22 June at 1900 EST. Total precipitation was 25 mm.

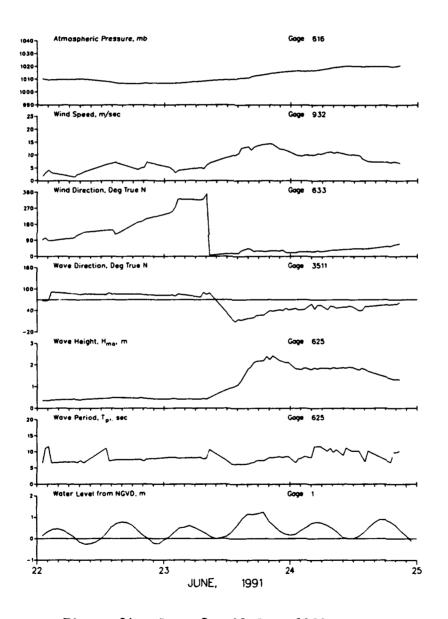


Figure 34. Data for 23 June 1991 storm

18-19 August 1991 - Hurricane Bob" (Figure 35)

73. Bob reached tropical storm intensity on 16 August while located close to Bermuda and was upgraded to a hurricane on 17 August. The storm continued to intensify as it rapidly moved up the east coast, developing into a Category 3 hurricane (winds of 50-58 m/s (111 to 130 mph) on the Saffir/Simpson hurricane scale) as the eye passed 25-30 miles (40-48 km) east of Cape Hatteras, NC early on 19 August. Continuing up the coast, the storm finally made landfall on the Rhode Island coast late on 19 August. The maximum H_{mo} (at Gage 630) of 4.83 m (T_{p} = 15.06 sec) was recorded at 2342 EST on 18 August. Maximum onshore winds (from the northeast) approached 15 m/s occurring several hours earlier at 1934 EST. Peak winds (from the northwest) exceeded 23 m/s near midnight on 18 August. This coincided with the minimum atmospheric pressure of 994.0 mb. Total precipitation was 43 mm.

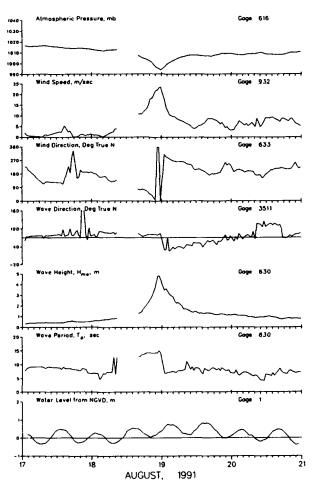


Figure 35. Data for Hurricane Bob, 18-19 August 1991

25 August 1991 (Figure 36)

74. A Canadian high-pressure system briefly produced storm waves at the FRF on 25 August. Maximum winds (from the northeast) exceeding 13 m/s peaked at 1708 EST on 25 August, with the maximum $H_{\rm mo}$ (at Gage 625) of 2.19 m ($T_{\rm p}$ = 6.40 sec) occurring several minutes later at 1742 EST.

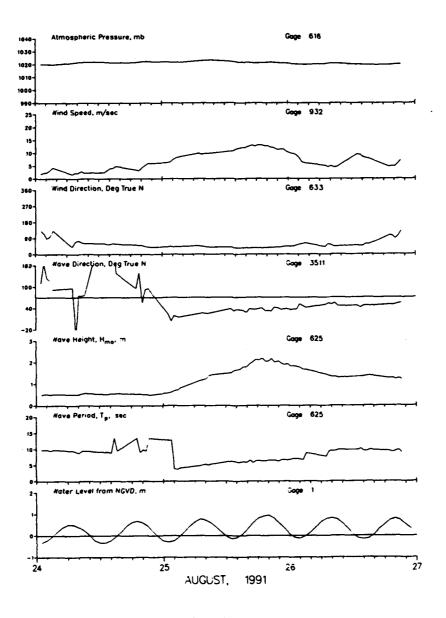


Figure 36. Data for 25 August 1991 storm

1-2 September 1991 (Figure 37)

75. A strong Canadian high-pressure system generated storm waves at the FRF on 1-2 September. Maximum winds (from the northeast) approached 15 m/s peaking at 1300 EST on 1 September with the maximum H_{mo} (at Gage 625) of 2.47 m (T_p = 8.00 sec) occurring several hours later at 1742 EST.

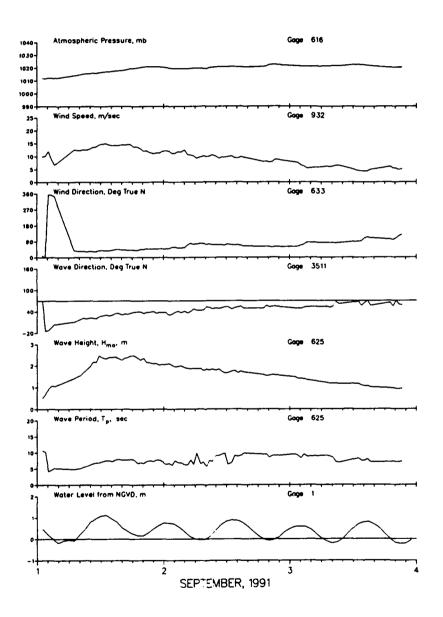


Figure 37. Data for 1-2 September 1991 storm

20 September 1991 (Figure 38)

76. A Midwestern high-pressure system briefly produced storm waves at the FRF on 20 September. Maximum winds (from the northwest) exceeding 16 m/s were recorded at 1000 EST on 20 September with the maximum $H_{\rm mo}$ (at Gage 625) of 2.28 m ($T_{\rm p}$ = 7.11 sec) occurring at 1216 EST.

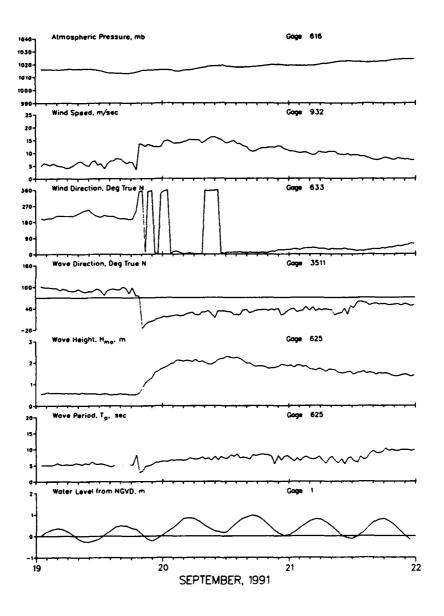


Figure 38. Data for 20 September 1991 storm

3 October 1991 (Figure 39)

77. Developing over southern Florida early on 1 October, this small coastal storm slowly moved up the eastern coast, being located off Cape Hatteras, NC on the morning of 3 October. Rapidly picking up speed, the storm was located off the Maine coast early the next day. The maximum H_{mo} (at Gage 625) of 2.34 m (T_p = 5.69 sec) occurred at 0916 EST on 3 October.

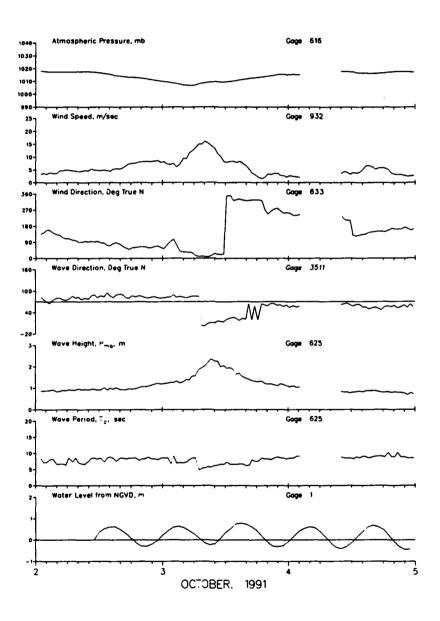


Figure 39. Data for 3 October 1991 storm

16-17 October 1991 (Figure 40)

78. Forming over Texas on 14 October this storm slowly travelled across the southeastern United States, moving into the Atlantic on 16 October. Located off South Carolina, the storm rapidly intensified beginning a northerly track up the coast. By 18 October the storm was located off the Maine coast. Peak onshore winds exceeding 15 m/s (from the northeast) were recorded at 2308 EST on 16 October with the maximum H_{mo} (at Gage 625) of 2.63 m (T_p = 7.31 sec) following at 2342 EST. The minimum atmospheric pressure of 1,004.7 mb occurred on 17 October at 0434 EST. Precipitation was 56 mm.

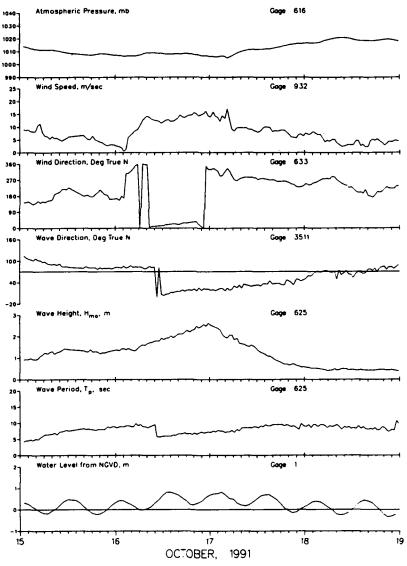


Figure 40. Data for 16-17 October 1991 storm

- 79. ("Halloween Storm") This major storm, which was similar in many respects to the 1962 "Ash Wednesday" storm, was actually a sequence of events which began with a hurricane. Early on 27 October, Hurricane Grace approached the southeastern U.S. coast. While still well out to sea, Grace curved to the north, following a track that paralleled the coast but kept her well offshore. By the morning of 28 October, Grace was located approximately 1,000 kilometers east of the North Carolina coast where she encountered a strong easterly moving Canadian high-pressure system. The collision of these two systems produced high onshore winds at the FRF. Augmented by these strong winds, large waves, which were produced well offshore by Hurricane Grace, continued to build as they approached the North Carolina coast; wave heights recorded at the FRF increased throughout the day. Grace continued to track north, finally being absorbed by a low-pressure system located off Nova Scotia late on 29 October. The merging of these two systems produced a huge storm which, contrary to normal storm tracks, proceeded to slowly move to the southwest. Early on 30 October the storm was off the New England coast and generating hurricane-force winds with a central atmospheric pressure of 988 mb as it continued its slow southwesterly course. By the morning of 31 October the storm was located well off the Maryland shore; although still strong, it had begun to weaken with its southwesterly movement greatly reduced. November 1 found the storm reversing its course and moving back out to sea as it continued to weaken. By the morning of November 2, the storm had curved back to the north; however, by the time the storm crossed the Maine coast, it had weakened considerably.
- 80. Although only a few oceanfront structures on the Outer Banks were completely destroyed, there was heavy damage to the primary dune system as well as extensive flooding and ocean overwash. Much of the sediment removed from the dunes was deposited inland burying most of an oceanfront road, while the flooding made many other roads impassable for over a week. Much heavier damage was reported to areas north of the Outer Banks, especially along the New England coast.
- 81. Maximum wind speeds at the FRF approached 18 m/s at 1600 EST on 28 October while the maximum H_{mo} (at Gage 630) of 5.93 m (T_p = 19.69 sec) occurred at 0016 EST on 31 October. The minimum atmospheric pressure at the

FRF only fell to 1,004.7 mb. This was a result of the storm center remaining well offshore. There was no precipitation at the FRF from this storm.

82. This storm encompassed several interesting features. Waves with an H_{mo} above 2.0 m (at Gage 625) lasted for 101 consecutive hours. The maximum T_p reached 21.33 sec on 30 October, while waves with T_p above 15 sec (normally only associated with hurricanes) were recorded both on 30 and 31 October, long after Hurricane Grace had passed. The storm surge at the FRF approached 0.7 m, with the highest tide level reaching +1.53 m (NGVD) on 31 October.

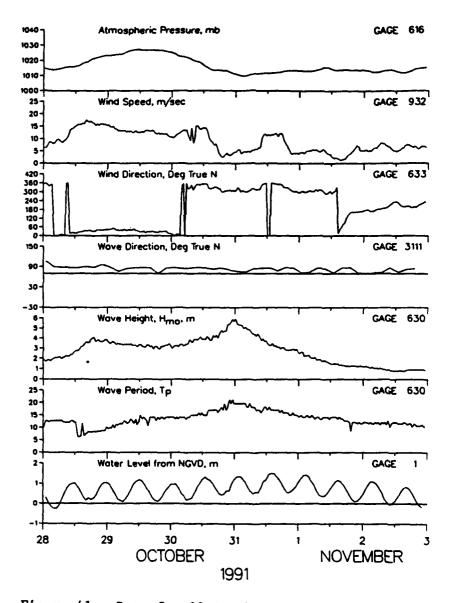


Figure 41. Data for 28 October-1 November 1991 storm

8-10 November 1991 (Figure 42)

83. Developing off Florida on 7 November, this storm slowly moved up the coast being located near Cape Hatteras, NC early on 10 November and reaching New England by 12 November. Maximum wind speeds (from the northeast) exceeded 21 m/s at 1600 EST on 9 November followed by the peak H_{mo} (at Gage 625), which reached 3.49 m (T_p = 12.19 sec) at 2234 EST. The minimum atmospheric pressure of 1,003.3 mb was recorded at 0508 EST on 10 November. Total precipitation was 39 mm.

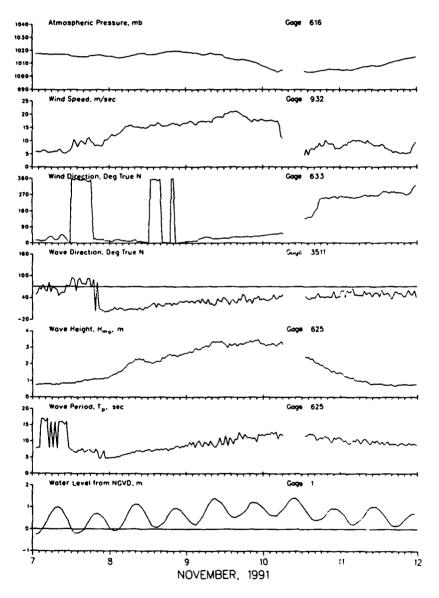


Figure 42. Data for 8-10 November 1991 storm

19 December 1991 (Figure 43)

84. A strong high-pressure system centered over the Great Lakes briefly generated storm waves at the FRF on 19 December. The peak wind speed (from the north-northwest) which surpassed 15 m/s was recorded at 1216 EST on 19 December. The maximum H_{mo} (at Gage 625) of 2.18 m (T_p = 7.31 sec) occurred several hours earlier at 1034 EST.

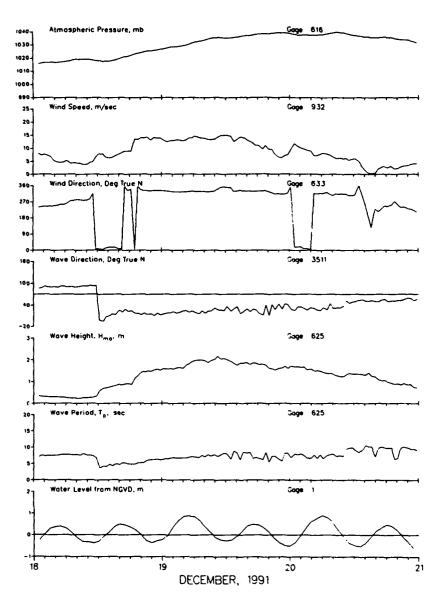


Figure 43. Data for 19 December 1991 storm

31 December 1991 (Figure 44)

85. Another strong high-pressure system centered over the Great Lakes again generated storm waves at the FRF for a brief time on 31 December. The peak wind speed (from the northeast) which exceeded 12 m/s, was recorded at 0734 EST on 31 December. The maximum H_{mo} (at Gage 625) of 2.07 m (T_p = 10.67 sec) occurred several hours $1\varepsilon \approx 2$ at 1742 EST.

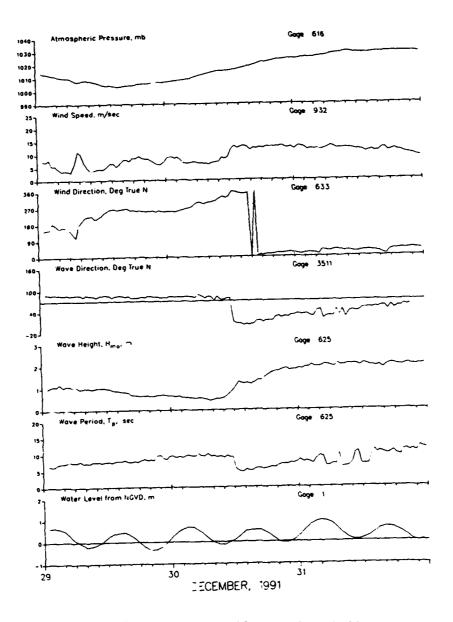


Figure 44. Data for 31 December 1991 storm

REFERENCES

Bingham, C., Godfrey, M. D., and Tukey, J. W. 1967. "Modern Techniques of Power Spectrum Estimation," IEEE Trans. Audio Electroacoustics, AU-15, pp 56-66.

Birkemeier, W. A., and Mason, C. 1984. "The CRAB: A Unique Nearshore Surveying Vehicle," <u>Journal of Surveying Engineering</u>, American Society of Civil Engineers, Vol 110, No. 1.

Field Research Facility. 1991 (Jan-Dec). "Preliminary Data Summary," Monthly Series, Coastal Engineering Research Center, US Army Engineer Waterways Experiment Station, Vicksburg, MS.

Grogg, W. E., Jr. 1986. "Calibration and Stability Characteristics of the Baylor Staff Wave Gage," Miscellaneous Paper CERC-86-7, US Army Engineer Waterways Experiment Station, Vicksburg, MS.

Miller, H. C. 1980. "Instrumentation at CERC's Field Research Facility, Duck, North Carolina," CERC Miscellaneous Report 80-8, US Army Engineer Waterways Experiment Station, Vicksburg, MS.

Miller, H. C., Birkemeier, W. A., and DeWall, A. E. 1983. "Effect of the CERC Research Pier on Nearshore Processes," <u>Coastal Structures '83</u>, American Society of Civil Engineers, Arlington, VA, pp 769-785.

US Department of Commerce. 1987. "Daily Weather Maps," Weekly Series, Washington, DC.

Welch, P. D. 1967. "The Use of Fast Fourier Transform for the Estimation of Power Spectra: A Method Based on Time Averaging Over Short Modified Periodograms," IEEE Trans. Audio Electroacoustics, AE-15, pp 70-73.

APPENDIX A: SURVEY DATA

- 1. Contour diagrams constructed from the bathymetric survey data are presented in this appendix. The profile lines surveyed are identified on each diagram. Contours are in 4-meter increments referenced to the National Geodetic Vertical Datum (NGVD). The distance offshore is referenced to the Field Research Facility (FRF) monumentation baseline behind the dune.
- 2. Changes in FRF bathymetry diagrams constructed by contouring the difference between two contour diagrams are also presented with contour intervals of 0.25 m. Wide contour lines show areas of erosion. Other areas correspond to areas of accretion. Although these change diagrams are based on considerable interpolation of the original survey data, they do facilitate comparison of the contour diagrams.

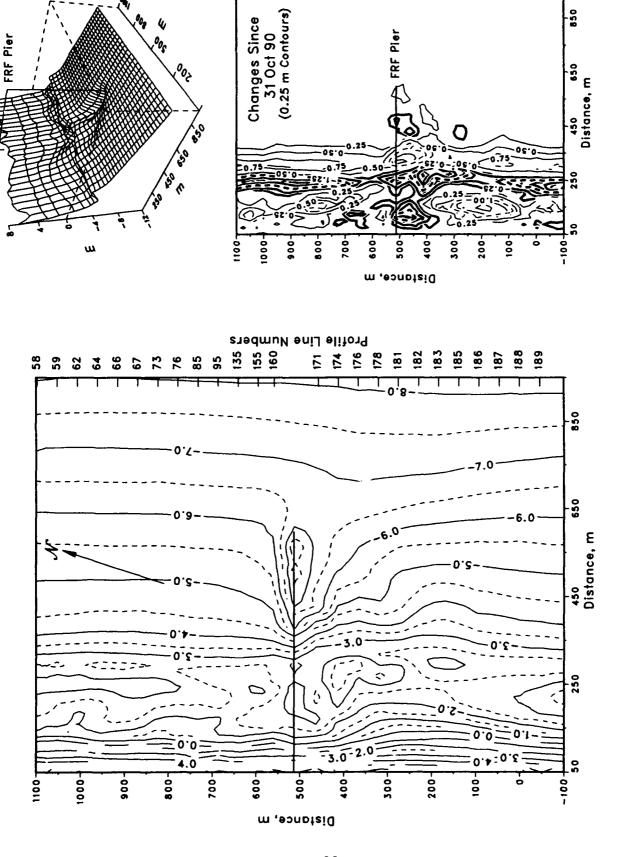


Figure Al. FRF Bathymetry 18 January 91 (depths relative to NGVD)

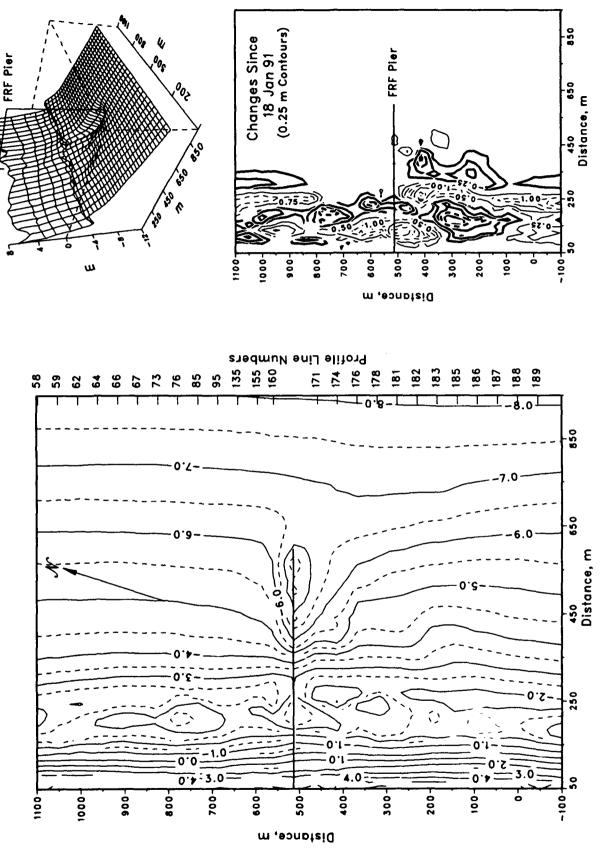


Figure A2. FRF Bathymetry 27 March 91 (depths relative to NGVD)

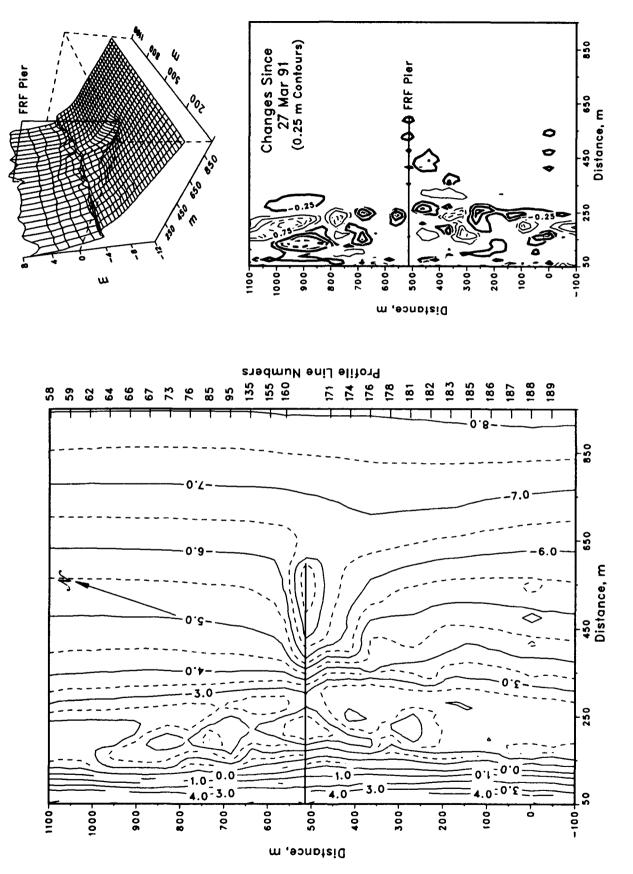


Figure A3. FRF Bathymetry 22 April 91 (depths relative to NGVD)

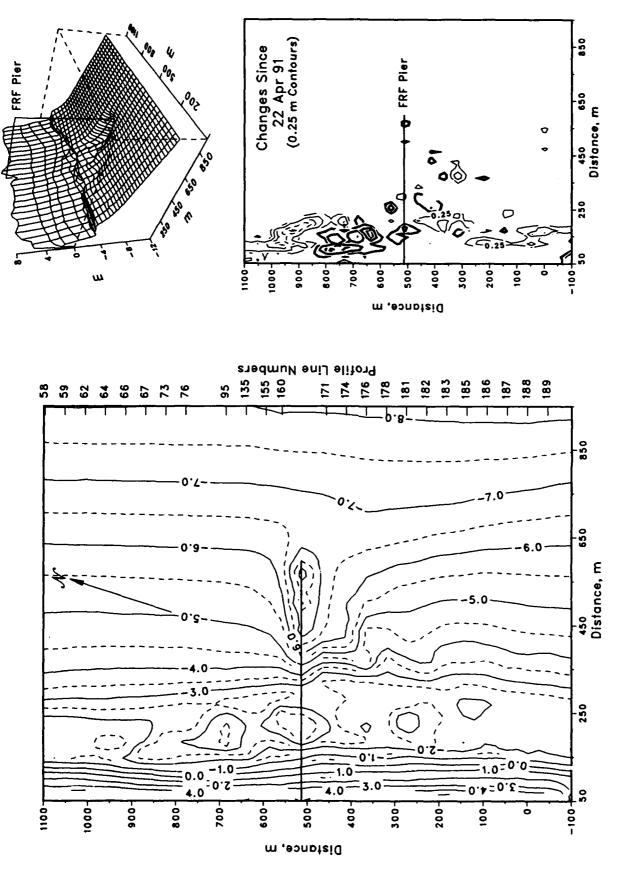


Figure A4. FRF Bathymetry 24 May 91 (depths relative to NGVD)

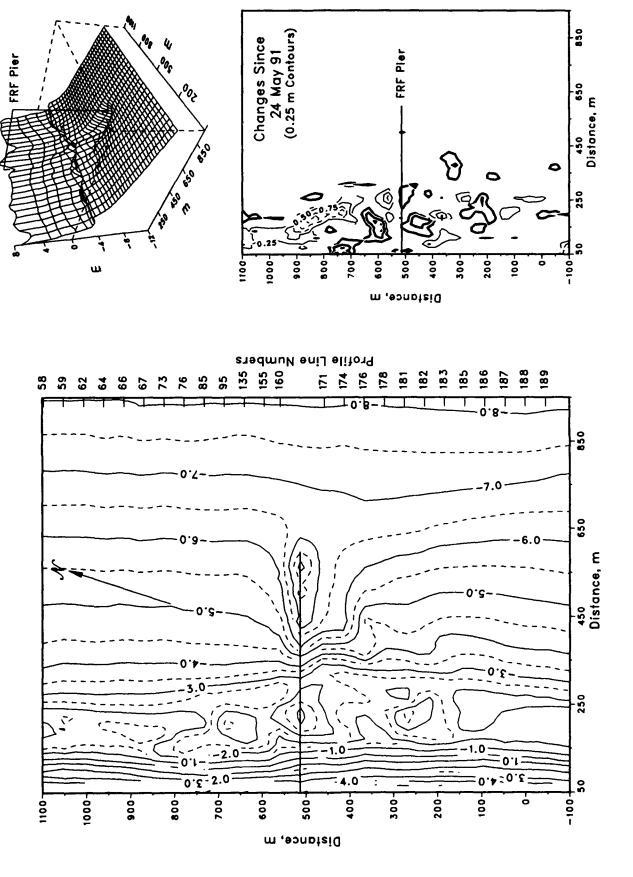


Figure A5. FRF Bathymetry 27 June 91 (depths relative to NGVD)

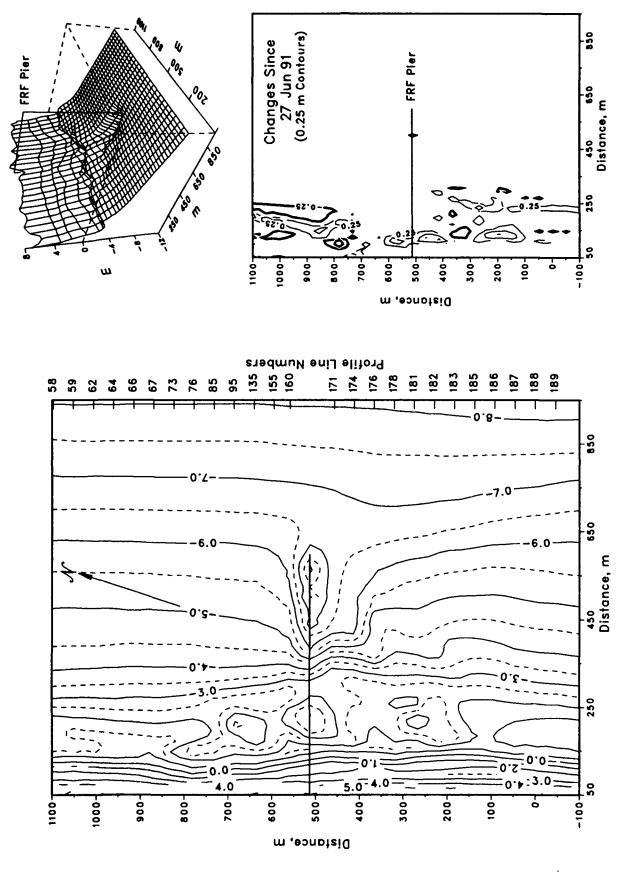


Figure A6. FRF Bathymetry 26 July 91 (depths relative to NGVD)

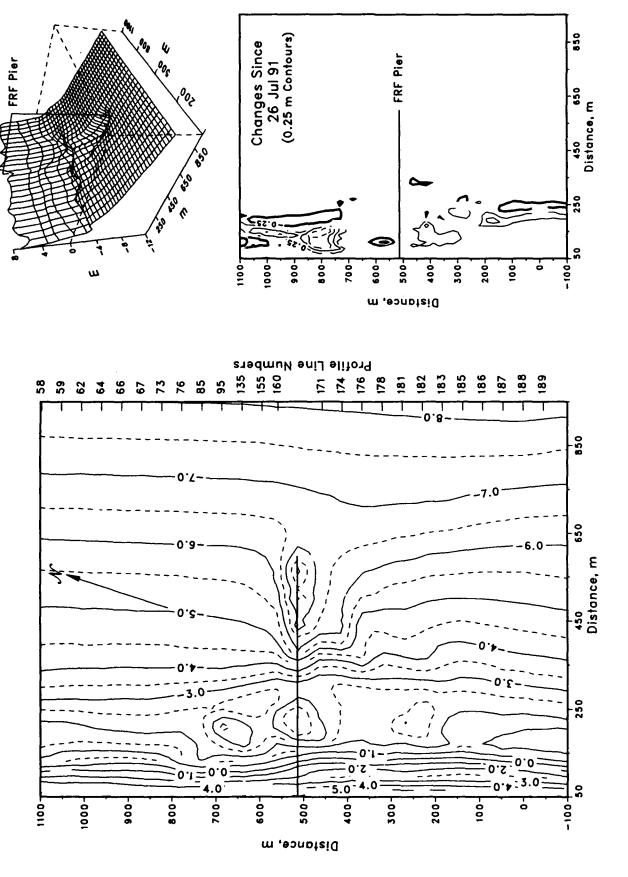


Figure A7. FRF Bathymetry 23 August 91 (depths relative to NGVD)

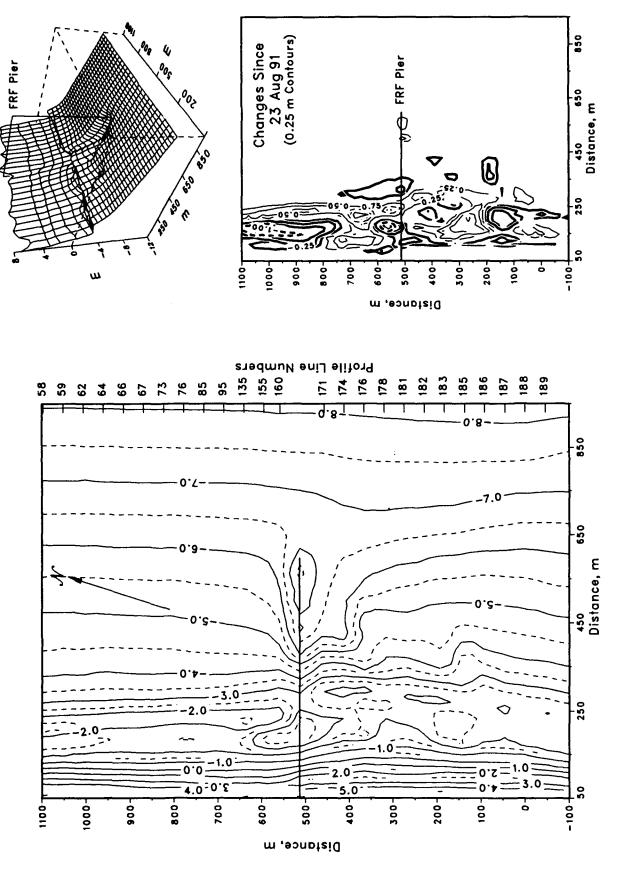


Figure A8. FRF Bathymetry 23 September 91 (depths relative to NGVD)

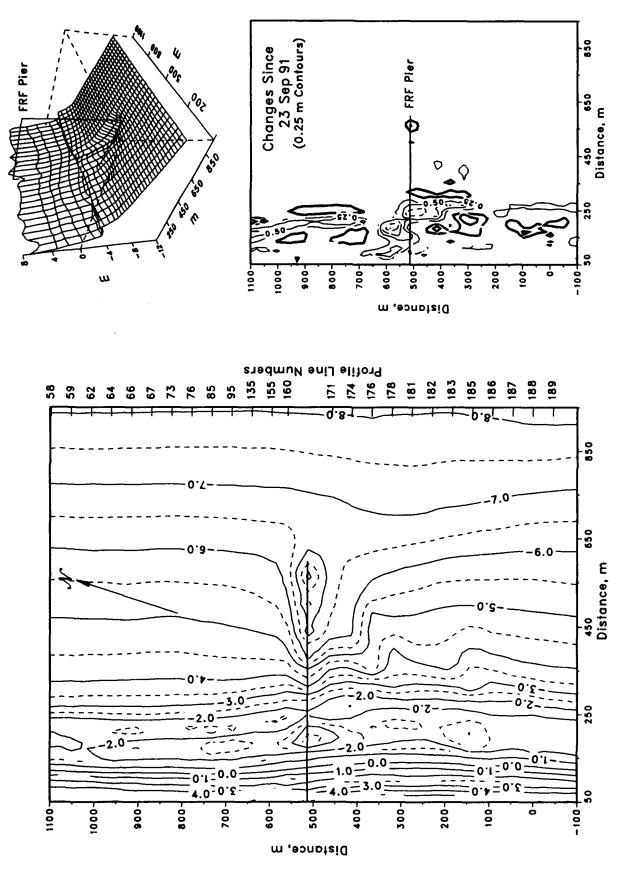


Figure A9. FRF Bathymetry 23 October 91 (depths relative to NGVD)

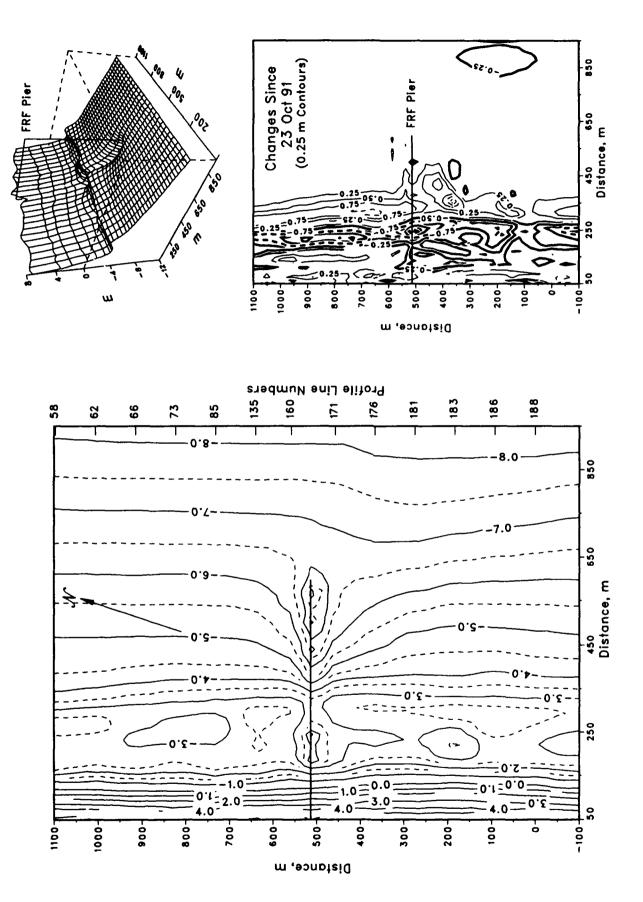


Figure A10. FRF Bathymetry 3 November 91 (depths relative to NGVD)

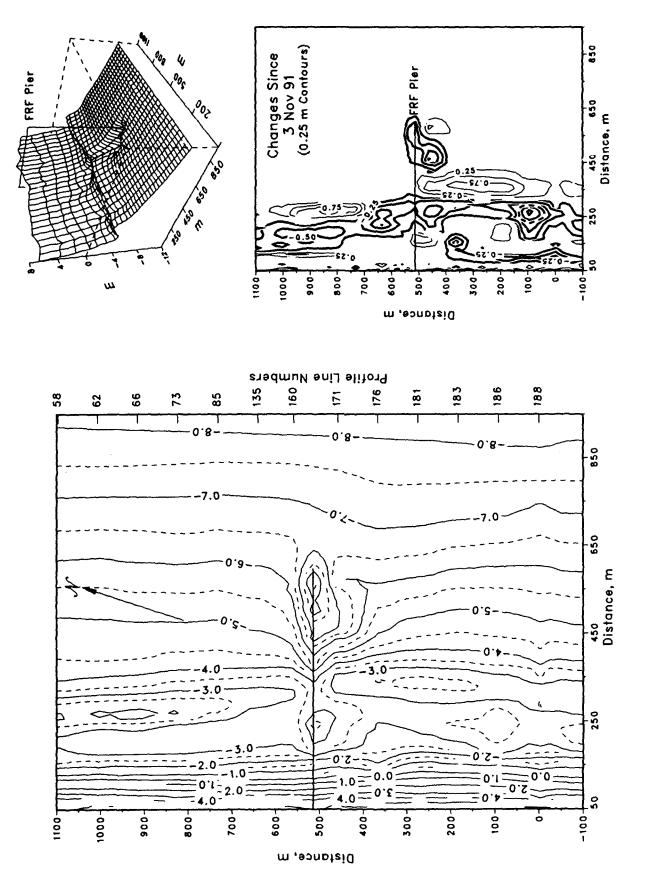


Figure All. FRF Bathymetry 12 November 91 (depths relative to NGVD)

Figure A12. FRF Bathymetry 18 December 91 (depths relative to NGVD)

Distance, m

APPENDIX B: WAVE DATA FOR GAGE 630

1. Wave data summaries for Gage 630 are presented for 1991 and for 1980 through 1991 in the following forms:

Daily H_{mo} and T_{p}

2. Figure B1 displays the individual wave height (H_{mo}) and peak spectral wave period (T_p) values, along with the monthly mean values.

Joint Distributions of $\ H_{mo}$ and $\ T_{p}$

3. Annual and monthly joint distribution tables are presented in Tables B1 and B2, and data for 1980 through 1991 are in Tables B3 and B4. Each table gives the frequency (in parts per 10,000) for which the wave height and peak period were within the specified intervals; these values can be converted to percentages by dividing by 100. Marginal totals are also included. The row total gives the number of observations out of 10,000 that fell within each specified peak period interval. The column total gives the number of observations out of 10,000 that fell within each specified wave height interval.

Cumulative Distributions of Wave Height

4. Annual and monthly wave height distributions for 1991 are plotted in cumulative form in Figures B2 and B3. Data for 1980 through 1991 are plotted in Figure B4.

Peak Spectral Wave Period Distributions

5. Annual and monthly peak wave period T_p distribution histograms for 1991 are presented in Figures B5 and B6. Data for 1980 through 1991 are presented in Figure B7.

Persistence of Wave Heights

6. Table B5 shows the number of times in 1991 when the specified wave height was equaled or exceeded at least once during each day for the duration (consecutive days). Data for 1980 through 1991 are averaged and given in Table B6. An example is shown below:

Height							Cons	ecut	ive	Day(s) or	Lon	ger						
	1	_2	_3	4	_5	_6		8	2	<u>10</u>	11	12	<u>13</u>	14	15	<u>16</u>	17	<u>18</u>	<u>19+</u>
0.5	18	15		14	13	12		11	10	9				8		7			
1.0	50	34	24	21	18	14	12	8	7	3			2						
1.5	41	19	8	6	2	1													
2.0	22	9	5	1															
2.5	10	5	2																
3.0	6	1																	
3.5		1																	
4.0	1																		

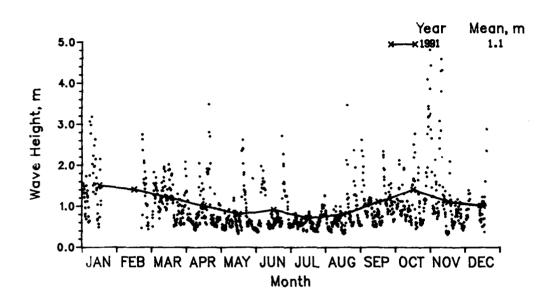
This example indicates that wave heights equaled or exceeded 1.0 m 50 times for at least 1 day; 34 times for at least 2 days; 24 times for at least 3 days, etc. Therefore, on 16 occasions the height equaled or exceeded 1.0 m for 1 day exactly (50 - 34 = 16); on 10 occasions for 2 days; on 3 occasions for 3 days, etc. Note that the height exceeded 1 m 50 times for 1 day or longer, while heights exceeded 0.5 m only 18 times for this same duration. This change in durations occurred because the longer durations of lower waves may be interspersed with shorter, but more frequent, intervals of higher waves. For example, one of the times that the wave heights exceeded 0.5 m for 16 days may have represented three times the height exceeded 1 m for shorter durations.

Spectra

7. Monthly spectra for the offshore Waverider buoy (Gage 630) are presented in Figure B8. The plots show "relative" energy density as a function of wave frequency. These figures summarize the large number of spectra for each month. The figures emphasize the higher energy density associated with storms, as well as the general shifts in energy density to different frequencies. As used here, "relative" indicates the spectra have been smoothed by the three-dimensional surface drawing routine. Consequently, extremely high- and low-energy density values are modified to produce a smooth surface. The figures are not intended for quantitative measurements; however,

they do provide the energy density as a function of frequency relative to the other spectra for the month.

- 8. Monthly and annual wave statistics for Gage 630 for 1991 and for 1980 through 1991 are presented in Table B7.
 - 9. Figure B9 plots monthly time histories of wave height and period.



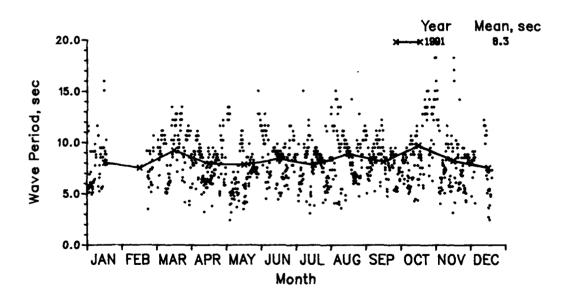


Figure B1. 1991 daily wave height and period values with monthly means for Gage 630

			Pe	ercent	Occur	nnual rence(1991 X100)	Gage 6 of Hei	30 ght and	d Perio	od		
Height(m)						Pe	riod(s	ec)					Total
	2.0- 			5.0- 		7.0- 	8.0- 8.9				14.0- _15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater	8 17	17 118 	17 285 84 17	50 596 437 176 25	50 655 269 227 118 50 8	84 579 193 101 50 50 25	319 982 537 92 42 34	243 840 218 76 25 .8	168 974 176 101 25 8	34 101 25 17 8 8 17 8	126 218 92 34 17 8 8	25 	1141 5365 2031 841 293 159 82 24 32 16

Height(m)			P	ercent	Occur		ry 199: X100) (riod(s:		e 630 ght and	d Perio	od		Tot
	2.0-	3.0- 3.9	4.0-	5.0- <u>5.9</u>	6.0- 6.9				10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99	•	:	: 164	328 1803 656	328 492 492	164	328 492	1311 164 328	492	:	164 164	:	16 262 344
2.00 - 2.49 2.50 - 2.99	•	•		164	432	328	492	164	492 164	:	:	•	213 82
3.00 - 3.49 3.50 - 3.99	•	•	:	•	:	164	432	:	164	:	:	•	49 32
.00 - 4.49	•	:	•	•	:	:	•	:		:	:	•	
1.50 - 4.99 5.00 - Greater Total	Ó	Ò	164	295i	1312	656	1312	1967	1312	Ò	328	Ö	
			P	ercent	0ccur	rence(ry 199: X100) (of Heig	e 630 ght and	d Perio	od		
Height(m)	2.0-	3.0-	4.0-	5.0-	6.0-		riod(s: 8.0-		10.0-	12.0-	14.0-	16.0-	Tot
	2.9	3.9	4.9	5.0	6.9	7.9	8.9	9.9	11.9	13.9	15.9	Longer	_
.00 - 0.49 .50 - 0.99	•	40Ô	•	•	•	40ô	40 0	800 800	40Ô			•	86 24
.00 - 1.49 .50 - 1.99	•	•		800 800	40Ô	1200 400	400 400	40Ô	•		:		24 24
2.00 - 2.49 2.50 - 2.99	:	:	:	•	800 400	40Ô	•	400	:	:	:	•	120
.00 - 3.49 .50 - 3.99	:	:	:	:		•	:	•	:	:	:	•	
.00 - 4.49 .50 - 4.99	•	•		•			:	•	:	•	•	•	
.00 - Greater Total	Ò	40Ò	Ò	1600	1600	2400	1200	2400	400	Ò	Ò	Ò	
			Pi	ercent	0ccur		h 1993 X100) d		e 630 ght and	d Perio	od		
Height(m)				-			riod(se						Tot
	2.0- 2.9	3.0- 	4.0- 4.9	5.0- <u>5.9</u>	6.0- <u>6.9</u>	7.0- 	8.0- <u>8.9</u>	9.0- 9.9	10.0- _11.9	12.0- _13.9	14.0- 15.9	16.0- Longer	
.00 - 0.49 .50 - 0.99 .00 - 1.49	•	8 5	169	85 678	169 424	85 169	254 847	678 508	1780 1102	85 85	424 508	•	364 449
.50 ~ 1.99 .00 ~ 2.49	•			254 85	339	169	339	254 ·	339 85				169 17
.50 - 2.99 .00 - 3.49	•	:	•	•	•	•	•	:	•	:		:	
.50 - 3.99 .00 - 4.49	:	•	•	•	•	•					•	•	
1.50 - 4.99	•	•	•			•		•	•	•	•	•	
i.00 - Greater Total	•	85	169	1102	932	423			3306	170	932	Ò	

(Continued)

Table B2 (Continued)

U-:			Po	ercent	0ccur	rence(il 199 X100) : riod(s	of Hei	e 630 ght and	d Perio	od		Tota
Height(m)	2.0- 2.9	3.0- 3.9	4.0- 4.9	5.0- 	6.0- <u>6.9</u>		8.0-	9.0-	10.0- _11.9	12.0- 	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99	•	167	167	667	1417	667	250 2000	250 583 167	1083	:	167	:	500 6918
1.00 - 1.49 1.50 - 1.99	:	:	:	333 167	333 333 83	83	500 167	83 83	:	:	:	:	1333 833 166
2.00 - 2.49 2.50 - 2.99 3.00 - 3.49	•	•		•		83 83	83			:			166 168
3.50 - 3.99 3.00 - 4.49	:	:	:	:	:		:	•	:		:	:	0.
1.50 - 4.99 5.00 - Greater	:	:	:	:	:	:	÷	:	:	:	:	÷	Ì
Total	Ò	167	167	1167	2166	916	3000	1166	1083	Ó	167	Ò	·
			Pe	ercent	0ccur	M rence(ay 199 X100)	l. Gag of Hei	e 630 ght and	d Peri	od		
Height(m)						Pe	riod(s	ec)					Tota
	2.0-	3.0-	4.0-	5.0- 5.9	6.0- 6.9	7.0~ 		9.0- 9.9	10.0- 11.9	12.0-	14.0- 15.9	16.0- Longer	
0.00 - 0.49		82	164	328	246		82	246	656	164	738	Longer	270
).50 - 0.99 .00 - 1.49	82	246	820 164	984 164	656 246	1557 82	328 164	410 82	328	82	246	•	5739 900
1.50 - 1.99 2.00 - 2.49	:	:		82	246	82	82		:	•	82	•	24 32
2.50 - 2.99 3.00 - 3.49	:		:	:	82	÷		:	:	:	:	•	8
3.50 - 3.99 1.00 - 4.49		•	•	:	:	:	:	:	:	:	:	:	
1.50 - 4.99		:		:	•	:	•	:	•		•	•	
5.00 - Greater Total	82	32 8	1148	1558	1476	172İ	65Ġ	73 8	984	246	1066	Ó	,
Height(m)			P:	ercent	0ccur		ne 199 X100) riod(s		e 630 ght an	d Peri	od 	·	Tota
	2.0- 2.9	3.0- 3.9	4.0- _4.9	5.0- 	6.0- <u>6.9</u>	7.0- <u>7.9</u>	8.0- <u>8.9</u>	9.0- <u>9.9</u>	10.0- 11.9	12.0- 13.9	14.0- _15.9	16.0- Longer	
).00 - 0.49).50 - 0.99	•		189	94 566	66 0	94 472	377 1415	566 1415	283 943	•	94	•	141 . 575
1.00 - 1.49 1.50 - 1.99	:	:	94	189 189	94 472	377 94	377	94	189 377	:		:	141 113
2.00 - 2.49 2.50 - 2.99	:	:	:	103	7/2	94 94	189	:		:	:	:	18: 18: 9:
3.00 - 3.49	:	:	:	:	:		:	:	:	:	:		
1.50 - 3.99 1.00 - 4.49	•	:	•	•	•		•	•	:	:	:	:	
1.50 - 4.99 5.00 - Greater	Ò	Ö					aaca					Ò	
Total	O	U	283	1038	1226	1131	2358	2075	1792	0	94	U	
						10	ntinue						

Table B2 (Continued)

Height(m)			P	ercent	0ccur	rence(ly 199 X100) riod(s	1. Gage of Heig ec)	e 630 ght and	d Perio	od		Tota
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- 6.9	7.0-	8.0-	9.0-	10.0- 11.9	12.0- _13.9	14.0- 15.9	16.0- Longer	
0 00 - 0.49 0.50 - 0.99 1.00 - 1.49	:	259	603	1293 86	172 948 86	345 690 86	1207 1638 172	345 1034	172 517	8Ġ	86 172	•	2327 7240 430
1.50 - 1.99 2.00 - 2.49	•	•	•	•	:	:	•	•	•	•		•	Ç
2.50 - 2.99 3.00 - 3.49 3.50 - 3.99	•		:	•	:	:	:	:	•	:		•	
.00 - 4.49	:	:	:	:	:	:	:	:	:	:	:	•	
4.50 - 4.99 5.00 - Greater Total	Ò	259	603	1379	1206	112İ	3017	1379	689	86	258	Ò	
			P	ercent	0ccur	Augu rence (st 199	1, Gage of Heig	e 630 oht and	i Peri	nd		
Height(m)							riod(s						Tota
	2.0- 		4.0- 4.9	5.0- 	6.0- 6.9	7.0- 	8.0- 8.9	9.0- <u>9.9</u>	10.0- _11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
.00 - 0.49 .50 - 0.99		163	488	325	81 976	163 244	488 407	569 1138	325 2439	163 163	163 163	•	195 650
.00 - 1.49 .50 - 1.99	•	•	81	81 81	163 163	81	407	163	:	:	:	:	97 24
.00 - 2.49 .50 - 2.99	:	•		•	81	81	•			81		•	24
.00 - 3.49 .50 - 3.99	:		·		8i	:	:		:	:		:	8
.00 - 4.49 .50 - 4.99	•	•	•	•	•		•	•	•	•	•	•	
.00 - Greater Total	Ò	163	569	487	1545	569	1302	187Ô	276 4	407	32Ġ	ò	
					S	eptembj	er 199	1. Gage of Hei	e 630				
Height(m)			P	ercent	Occur		X100) riod(s		ght and	d Peri	od 		Tot
	2.0- 2.9	3.0- <u>3.9</u>	4.0- <u>4.9</u>	5.0- 	6.0- 6.9	7.0- -7.9	8.0- 8.9	9.0- 9.9	10.0- _11.9	12.0- _13.9	14.0- _15.9	16.0- Longer	
.00 - 0.49 .50 - 0.99	:		84	42 0	420	1092	1176	1176	168 756		84	•	16 520
.00 - 1.49 .50 - 1.99	•	•	•	672 84	168 252	336 336	1429 84	504 84	168	•		•	327 84 42
.00 - 2.49 .50 - 2.99	•		:	•	252	84 84	84	•		•		•	8
.00 - 3.49 .50 - 3.99	:	:	:	•	:	:	:	•	•	:	•	•	
.00 - 4.49 .50 - 4.99		•		•	:		:	•	•		•	•	
.00 - Greater Total	Ó	Ò	84	1176	1092	1932	2773	1764	1092	Ò	84	Ò	
						10-	ntinue	۸.					

Table B2 (Concluded)

Height(m)			P	ercent	0ccur	rence(er 199 X100) (riod(s	1, Gago of Heig	e 630 ght an	d Perio	od		Tota
ne gnt (m)	2.0-	3.0-	4.0- 4.9	5.0-	6.0- 6.9	7.0-	8.0-	9.0-	10.0-	12.0-	14.0- 15.9	16.0- Longer	1016
).00 - 0.49).50 - 0.99			164	246	328	164 164	82 1066	656	82 0	492	82 738		328 467
1.00 - 1.49 1.50 - 1.99	:	•	82	328 246	410 246	82 164	738 164	246 82	82 82	82 82	82 246	•	205 131
2.00 - 2.49 2.50 - 2.99	•	•		82	82 246	82	82	•	•	82	82	•	32 41
1.00 - 3.49 1.50 - 3.99			:					82		164 82	82 82	82 ·	41 16
.00 - 4.49 .50 - 4.99	:	:	:	•	•	:	82	•	:	:	•	82 82	16 8
i.00 - Greater Total	Ò	Ò	246	902	1312	656	2214	1066	902	984	1394	82 328	8
Height(m)			P	ercent	0ccur	rence(er 199 X100) riod(s	1. Gage of Heig	e 630 ght and	d Peri	od		Tot
•	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- 6.9				10.0-	12.0-	14.0- 15.9	16.0- Longer	
.00 - 0.49		85		85			763	339	85		85	254	169
0.50 - 0.99 .00 - 1.49	•	•	254 85	1186 508	508 508	678 254	1017 169	424 254	424 85	85 85	254	•	457 220
1.50 - 1.99 2.00 - 2.49	•	:	:	169	169 169	85	85		8 5	85	85		50 33
1.50 - 2.99 1.00 - 3.49 1.50 - 3.99	:	:	:	:	85 ·	85 85	85	:	•	:		•	25 8
.00 - 4.49 .50 - 4.99	:	:	:	:	:	:	:	85 85	85	:	·	:	17 8
.00 - Greater Total	Ó	85	339	1948	1439	1187	2119	1187	76 4	255	424	25 4	_
			ρ	ercent	0ccur	Decemb nense(er 199 X100)	1. Gag	e 630 gh+ an	d Peri	od		
Height(m)		·					riod(s						Tot
	2.0- 2.9	3.0- 3.9	4.0- _4.9		6.0- 6.9	7.0- <u>7.9</u>	8.0- 8.9	9.0- _9.9	10.0- _11.9	12.0- _13.9	14.0- 15.9	16.0- Longer	
.00 - 0.49 .50 - 0.99 .00 - 1.49	244 244	488	244 488	244 732	97 6	244 732	1220 732	488 244	1707		244	•	48 561 317
.50 - 1.99 .00 - 2.49	:	•	244	:	244				:	•		•	24 24
.50 - 2.99 .00 - 3.49		:	:			244	:	:	:	:	:	•	24
.50 - 3.99 .00 - 4.49	:	:	:			•	:			•			
.50 - 4.99 .00 - Greater	•	•	•	•	•	1220	•	•		•	•	Ò	

(Sheet 4 of 4)

			P	ercent	Occur	Annual rence(:	1980- X100)	1991, of Hei	Gage 6: ght an	30 d Peri	od		
Height(m)						Pe	riod(s	ec)					Total
	2.0- 	3.0- 3.9	4.0- _4.9	5.0- 	6.0- 6.9	7.0- 	8.0- 8.9	9.0- _9.9	10.0- _11.9	12.0- _13.9			
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater	27 37 	14 136 9 	26 255 143 13 1 	60 509 405 164 24 1	86 592 424 245 95 12 1	114 526 251 111 67 32 12 1	332 882 284 83 54 18 12 6 2	278 744 212 78 37 13 12 7 4 1	189 801 322 126 59 32 14 11 7 2	66 140 40 32 27 10 5 4 1	126 229 121 72 36 24 8 5 3	5 16 3 4 1 1 1 1 1 34	1323 4867 2214 928 401 143 65 34 18

 $Table \ B4$ Monthly Joint Distribution of $\ H_{mo}$ versus $\ T_p$ (All Years)

			Po	ercent	J. Occur	anuary rence(1980- X100)	1991, (of He i	Gage 6: ght and	30 d Perio	od		
Height(m)						Pe	riod(s	ec)					Total
-	2.0- 2.9	3.0- 3.9	4.0- <u>4.9</u>	5.0- <u>5.9</u>	6.0- 6.9	7.0- 	8.0- 8.9	9.0- <u>9.9</u>	10.0- _11.9	12.0- 13.9	14.0- _15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99	88 72	8 207	8 231	80 406	72 406	40 351	151 351	247 709	215 829	48 104	96 223	•	1053 3889
1.00 - 1.49 1.50 - 1.99	:	16	159 32	598 335	534 414	247 183	207 96	199 104	486 231	24 24	56 48	8	2534 1467
2.00 - 2.49 2.50 - 2.99	:	•	•	32	175 16	183 64	96 64	32 16	104 64	32 16	24 40	8	686 280
3.00 - 3.49 3.50 - 3.99	•	:	•	:	:	16	24	8	32	•	:	•	80 0
4.00 - 4.49 4.50 - 4.99 5.00 - Greater	•	:	•	:	:	•	•	:	8 8	:	:	•	0 8 8 0
Total	16Ò	23i	43 0	145i	1617	1084	989	1315	1977	248	487	16	Ū
			Po	ercent					Gage 63 ght and		od		
Height(m)						Pe	r:od(s	ec)					Total
	2.0- 	3.0- 3.9	4.0- <u>4.9</u>	5.0- 	6.0- <u>6.9</u>	7.0- 	8.0- <u>8.9</u>	9.0- 9.9	10.0- _11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99	9 52	96	9 175	44 419	61 471	44 314	87 497	79 689	79 1003	26 17	105 166	ġ	543 3908
1.00 - 1.49 1.50 - 1.99	:	9	131	646 227	620 358	253 183	305 113	332 113	532 192	70 52	201 96	:	3099 1343
2.00 - 2.49 2.50 - 2.99	:	•	:	79 9	166 17	44 52	35 17	79 9	79 96	44 17	96 61	ġ	622 287
3.00 - 3.49 3.50 - 3.99 4.00 - 4.49	:	•	:	:		17	9	26 9 9	26 9 35	17	17 9 9	•	112 27 53
4.50 - 4.99 5.00 - Greater	:	:		:	:	:	9			:		•	9 9
Total	6i	105	324	1424	1693	907	1072	1345	205i	243	76Ò	18	j
					,	K arch	1980-	1991. (Gage 6:	30			
			Pe	ercent	0ccur	rence(X100) (of Hei	ght and	Peri	od		
Height(m)	2.0- 2.9	3.0- _3.9	4.0- 4.9	5.0- 	6.0- 	7.0- 7.9	riod(s 8.0- 8.9	9.0-	10.0- _11.9	12.0-	14.0-	16.0- Longer	Total
0.00 - 0.49	7	_3.3	_ 7	15	37	37	103	29	125	66	118	Luiger	544
0.50 - 0.99 1.00 - 1.49	7	74 7	169 214	434 434	420 486	398 331	611 368	700	898 663	118 52	221 309	•	4050
1.50 - 1.99 2.00 - 2.49	:	:	7	243 22	265 66	110 44	103 103	287 155 52 7	243 133	66 29 15	103 88		3151 1295 537 162
2.50 - 2.99 3.00 - 3.49		•		:	22	15 15	22	7 15 15	44 44	15 7	37	•	162 102
3.50 - 3.99 4.00 - 4.49		:	:	:	•	•	Ż	15 15	52 15 15		15 22		102 82 59 15
4.50 - 4.99 5.00 - Greater Total	14	8i	397	1148	1303	950	1324	1275	2232	353	920	Ö	15

(Continued)

(Sheet 1 of 4)

Table B4 (Continued)

Height(m)			Po	ercent	0ccur	rence(x100) (riod(s	of Heig	Sage 63 ght and	d Perio	od		Tota
	2.0-	3.0- 3.9	4.0- <u>4.9</u>	5.0- <u>5.9</u>	6.0- <u>6.9</u>		8.0-	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
).00 - 0.49).50 - 0.99 00 - 1.49	8 68	173 8	15 249 106	45 430 226	30 618 407	23 497 309	264 859 369	203 844 324	151 1070 294	75 219	75 377 143	:	897 5404 2239
.50 - 1.99 2.00 - 2.49	:	•		158 38	158 60	90 8	106 45	106 60	166 45	53 23 23	83 8	:	2239 890 287
2.50 - 2.99 3.00 - 3.49 3.50 - 3.99	:		:	•	8	23 30 8	30 15 30	15 23	30 23	23	15		144 91
1.50 - 3.99 1.00 - 4.49 1.50 - 4.99	:	:	:	•	:	•	8	ė	:	:	:	•	9:
5.00 - Greater Total	76	189	37 0	897	128i	988	1726	1583	1779	416	70i	Ò	(
			p	ercent	Occur	May rence!	1980- x1001	1991, (of Hei	Gage 6	30 1 Perio	nd		
Height(m)						-	riod(s						Tota
	2.0- 	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- 6.9	7.0- 7.9		9.0- 9.9			14.0- 15.9	16.0- Longer	
).00 - 0.49).50 - 0.99	7 22	22 192	52 377	96 637	148 585	141 888	392 1214	266 888	215 681	52 104	133 215		152 580
1.00 - 1.49 1.50 - 1.99		7	133	244 59	333 74	207 44	370 104	215 59	266 89	15	74	•	186
2.00 - 2.49 2.50 - 2.99	•		:	15	44 22	52 7	7 7	30 7	7	22 22 15 7	59 22 7 7		19 7
3.00 - 3.49 3.50 - 3.99 1.00 - 4.49	•	•	•	•		•		•	•	•		•	19 7 1
1.50 - 4.99 5.00 - Greater	:											:	:
Total	29	221	569	1051	1206	1339	2094	1465	1265	237	517	0	
Height(m)			Р	ercent	0ccur	rence(1980- X100) riod(s	1991, of Hei ec)	Gage 6 ght an	30 d Peri	od		Tot
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- 6.9	7.0-	8.0-	9.0-	10.0- 11.9	12.0- 13.9	14.0- _15.9	16.0- Longer	
).00 - 0.49).50 - 0.99	24 48	32 217	48 354	129 651	201 723	346 683	707 1672	547 989	209 523	40 129	32 48		231 603
1.00 - 1.49 1.50 - 1.99	:	8	88 16	225 56	177 105	177 56	201 32	105 16	96 96	:	40 48	•	111
2.00 - 2.49 2.50 - 2.99 3.00 - 3.49	:	•	:		24	16	48	8		:	:	:	9
3.50 - 3.99 3.00 - 4.49	•	:	:	:	:	:		:	:	:		•	42 9
1.50 - 4.99 5.00 - Greater Total	72	257	506	106i	1230	1286	2660	1665	924	169	168	Ö	
10001	,,	EJI	500	1001	1130			1003	7 .7		100	•	

Table B4 (Continued)

Height(m)			Po	ercent	0ccur		(100)	of Heig ec)	ght and	J Perio	od		Tota	
	2.0-	3.0- 3.9	4.0- _4.9	5.0- 5.9	6.0- 6.9	7.0-	8.0-	9.0- <u>9.9</u>	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer		
0.00 - 0.49 0.50 - 0.99	8 31	16 148	47 336	86 703	203 906	320 805	1008 1469	680 898	266 406	94 211	195 125	16 63	2939 6101	
1.00 - 1.49 1.50 - 1.99 2.00 - 2.49	•	16 ·	63	195 47	227 8	86 16	125 23	39 16	39 39	:	:	:	790 149 16	
2.50 - 2.99 3.00 - 3.49	:	:	•	8	•	•	8	•	•	:	•	•	0	
3.50 - 3.99 1.00 - 4.49	:	:	:	:	:		:		:	:	·			
1.50 - 4.99 5.00 - Greater				•			•			•		•	Ć	
Total	39	180	446	1039	1344	1227	2633	1633	750	305	320	79		
Height(m)		August 1980-1991, Gage 630 Percent Occurrence(X100) of Height and Period Period(sec)												
neignt(m)	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- 6.9	7.0- 7.9	8.0-	9.0-	10.0-	12.0-	14.0- 15.9	16.0- Longer	Tota	
0.00 - 0.49 0.50 - 0.99	23 38	23 92	54 230	107 553	146 844	192 698	583 1266	507 867	353 821	77 153	100 315	38	2165 5915	
1.00 - 1.49 1.50 - 1.99	:	8	130	307 69	261 138	184 54	223 31	123 15	84 15	15	31 31	:	1366	
2.00 - 2.49 2.50 - 2.99	:	•	:	15	31 8	15	15 15	:	31	8	8 8	:	353 123 39 32 8 0	
3.00 - 3.49 3.50 - 3.99	:	•	:	:	8	8	8	ġ	8	•	•	•	32 8	
4.00 - 4.49 4.50 - 4.99 5.00 - Greater	:	:	:	:	:	:	:	:	:	:	:		Č	
Total	6 i	123	414	105i	1436	115i	214İ	1520	1320	253	493	38	•	
Height(m)					Occur	rence(X100) riod(s		ght an	d Peri			Tota	
	2.0- 2.9	3.0- 3.9	4.0- _4.9	5.0- <u>5.9</u>			8.0- _8.9	9.0- _ 9. 9	_11.9	12.0- 13.9	14.0- _15.9	16.0- Longer		
0.00 - 0.49 0.50 - 0.99	8	8 107	8 176	31 405	23 534	15 588	107 893	244 779	214 1000	92 145	84 282	8 .	842 4909	
l.00 - 1.49 l.50 - 1.99	:	8	84 8	466 137	466 282	313 145 53	496 92	237 115	328 61	92 23	160 107	8 8	4909 2658 978	
.00 - 2.49 .50 - 2.99	•	:	:	31	92	46	76 23	23 8	61	61 8	61 8	•	458 93 40 24	
3.00 - 3.49 3.50 - 3.99	•	:	:	:	:	8	:	8	8 8	8 8	8 8	•	24	
1.00 - 4.49	:	:	:	:	:	:	:	:	:		:		(
1.50 - 4.99 5.00 - Greater				107Ò	1397	1168	1687	1414	1680	445	71 8	24		

(Sheet 3 of 4)

Table B4 (Concluded)

Height(m)			P	ercent		rence(1991, (of Heig			od		Tota
ne rgnc(m)	2.0-	3.0-	4.0-	5.0- 5.9	6.0- 6.9	7.0- 7.9			10.0- _11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	1014
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater	29 29 	59 : : : :	169 169 29	353 588 235 22	44 382 360 375 118 37	73 316 198 125 162 96 29	169 683 220 88 66 29 7 7 7 7	125 507 287 103 81 59 7 22 7	198 926 411 169 140 44 15	29 176 81 103 44 22 15 22	118 353 191 206 66 66 37 7	7 29 7 7 7 7	785 3960 2505 1462 706 353 117 58 36
			P	ercent		rence(X100)	1991, (of Hei			od		
Height(m)	2.0-	3.0-	4.0-	5.0-	6.0-		<u>riod(s</u> 8.0-	9.0-	10.0-	12.0-	14.0-	16.0-	Tota
	2.9	_3.9	4.9	5.9	6.9	_7.9	8.9	9.9	_11.9	_13.9	<u>15.9</u>	Longer	
0.00 - 0.49 0.50 - 0.99 0.00 - 1.49 0.50 - 1.99 0.50 - 2.49 0.50 - 2.99 0.50 - 3.49 0.50 - 3.99 0.50 - 4.49 0.50 - 4.99 0.50 - Greater	43 43 	35 87 17 	26 364 260 17 	26 641 511 208 26 	43 571 684 329 121 9 	104 476 398 199 121 35 9	277 511 277 121 113 9 17 9	190 537 251 69 35 17 43 9 9	95 606 268 104 26 43 35 9	61 121 43 52 17 9 17 9	199 121 104 9 9 17 9 9 	26 43 26 9	1122 4121 2833 11117 466 133 877 27
Height(m)			Po	ercent		rence()		1991, (of Heig			od		Tota
	2.0- 2.9	3.0- 3.9	4.0-	5.0- 5.9	6.0- <u>6.9</u>	7.0- 7.9	8.0- _8.9	9.0- 9.9	10.0- 11.9	12.0- _13.9	14.0- _15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 0.00 - 1.49 0.50 - 1.99 0.00 - 2.49 0.50 - 2.99 0.50 - 3.49 0.50 - 3.99 0.50 - 4.49 0.50 - 4.99	81 36 	27 181	45 244 199 27 18	63 487 469 217	18 650 605 487 280	27 235 325 144 117 45 9	108 442 226 90 36 63 27	217 469 135 63 45 18 18	126 830 406 99 72 54 18 27	135 171 36 9 45	280 271 135 63 54 27 9	9 36	1136 4052 2536 1199 667 144 117 81
.00 - Greater Total	117	208	533	1236	2040	902	992	992	9 1650	9 414	866	45	27

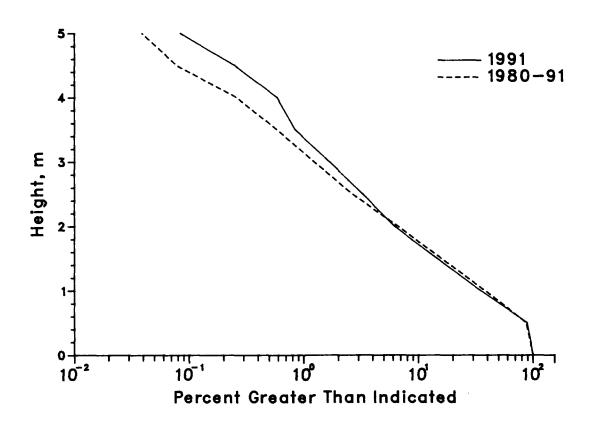


Figure B2. Annual cumulative wave height distributions for Gage 630

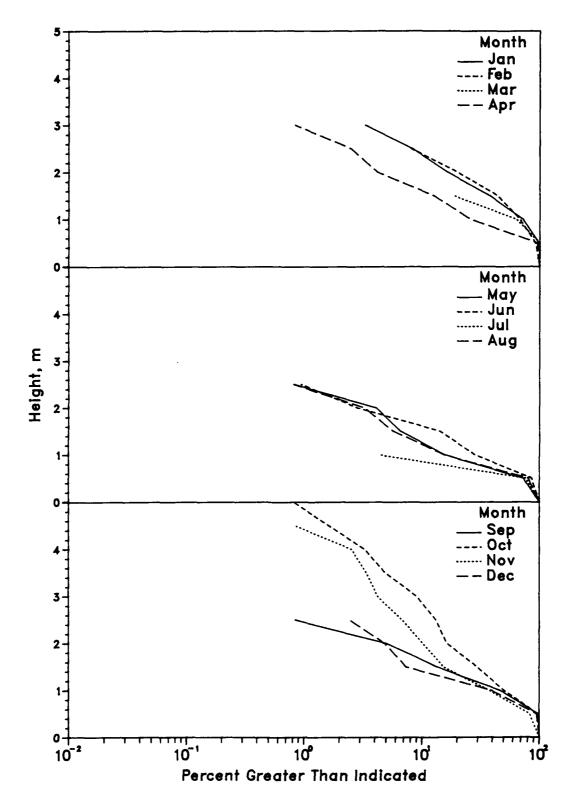


Figure B3. 1991 monthly wave height distributions for Gage 630

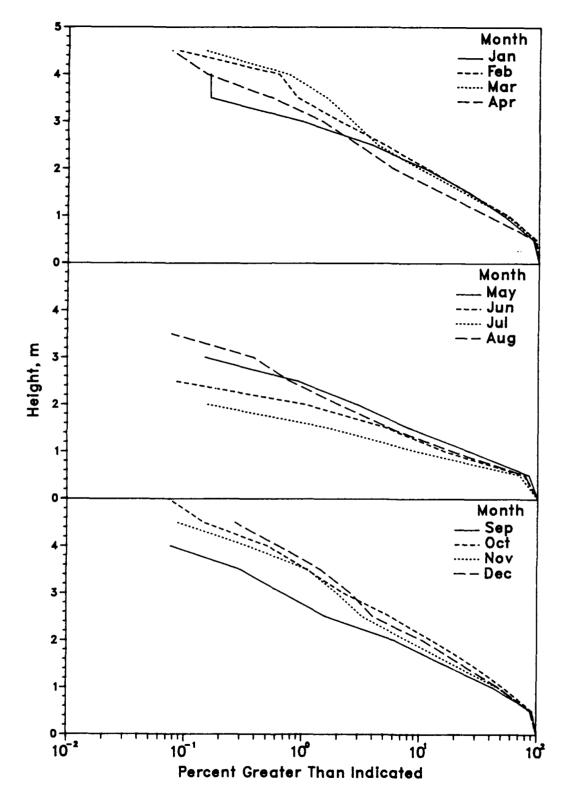


Figure B4. 1980-1991 monthly wave height distributions for Gage 630

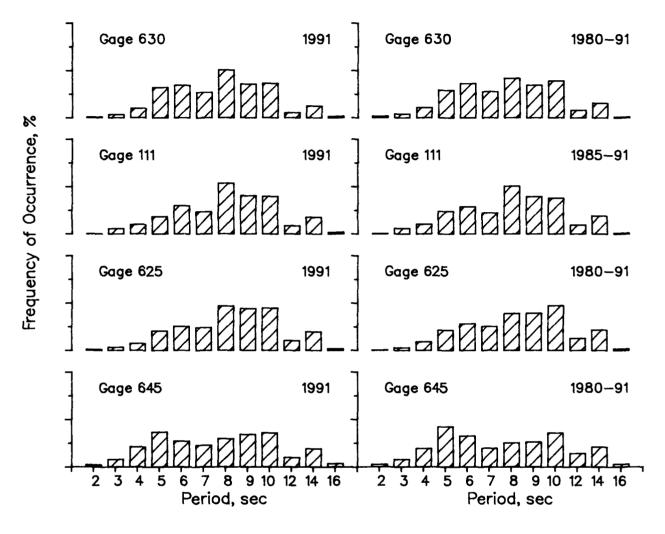


Figure B5. Annual wave period distributions for all gages

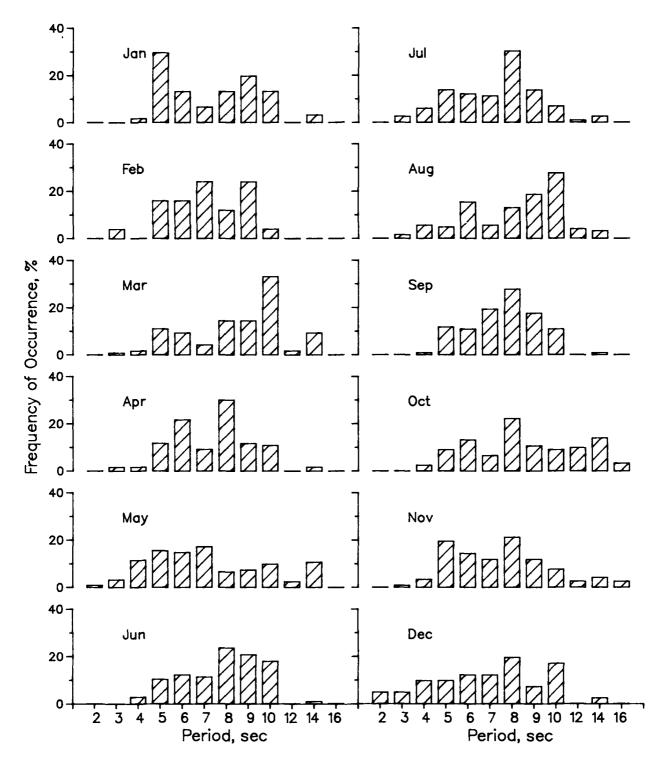


Figure B6. 1991 monthly wave period distributions for Gage 630

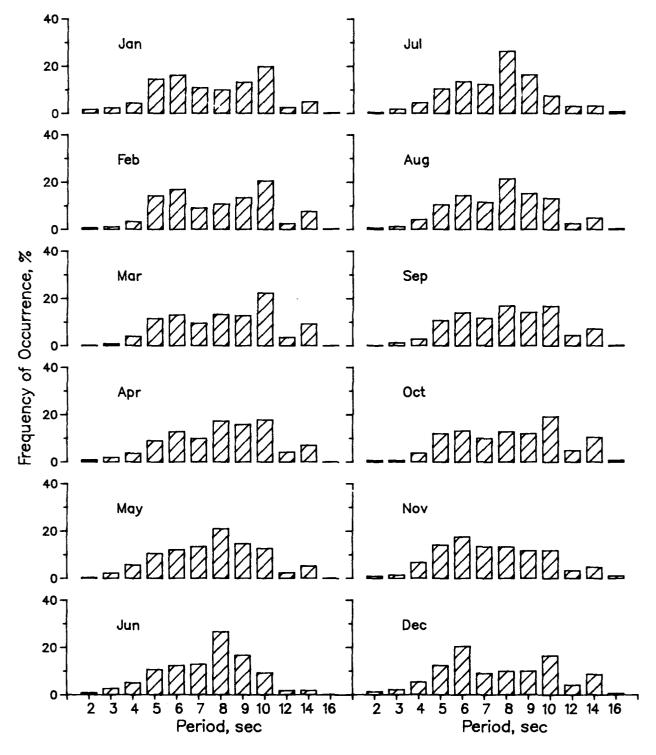


Figure B7. 1980-1991 monthly wave period distributions for Gage 630

Table B5 1991 Persistence of H_{mo} for Gage 630

Height							Cons	ecut	ive ()ay(s) or	Lon	ger						
(m)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19+
0.5		14	13			15		12		10	9	8	6					5	4
1.0	52	37	28	20	13	8	4	3	2				1						
1.5	42	25	12	5		2	1												
2.0	22	10	3		2	1													
2.5	12	5	3		1														
3.0	5		3	1															
3.5	3	2																	
4.0	3	2																	

Height							Cons	ecut	ive I)ay(s) or	Lon	ger						
(m)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19+
0.5	20	18	16	15		14	12		11	10		9	8	7	6	5			4
1.0	51	34	25	17	14	10	7	5	4	3		2					1		
1.5	39	22	11	6	4	2			1										
2.0	22	11	4	2		1													
2.5	11	5	2																
3.0	5	2	1																
3.5	3	1																	
4.0	2	1																	

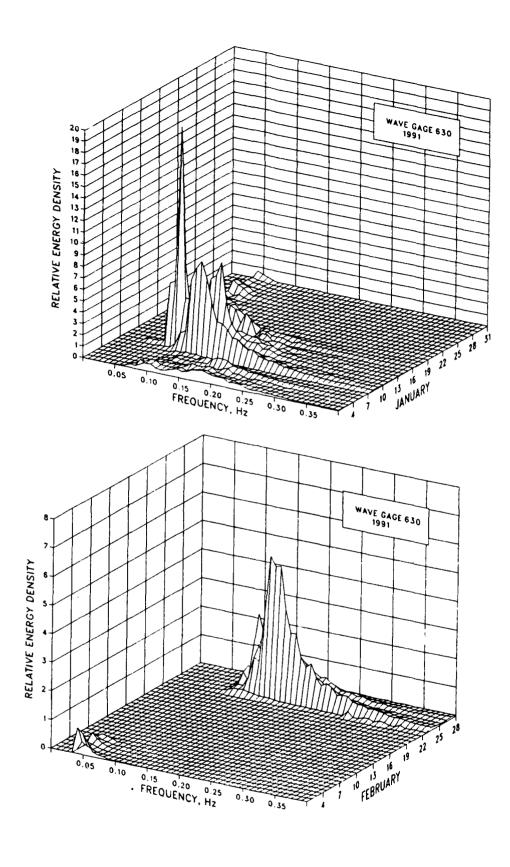


Figure B8. 1991 monthly spectra for Gage 630 (Sheet 1 of 6)

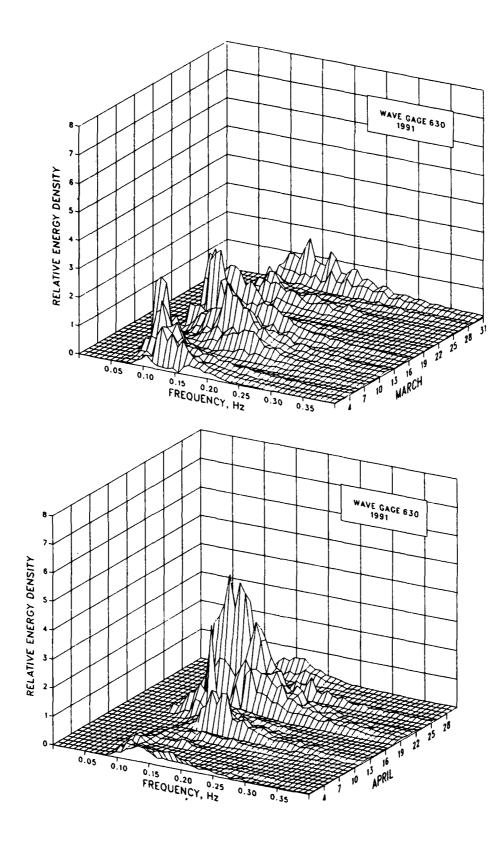


Figure B8. (Sheet 2 of 6)

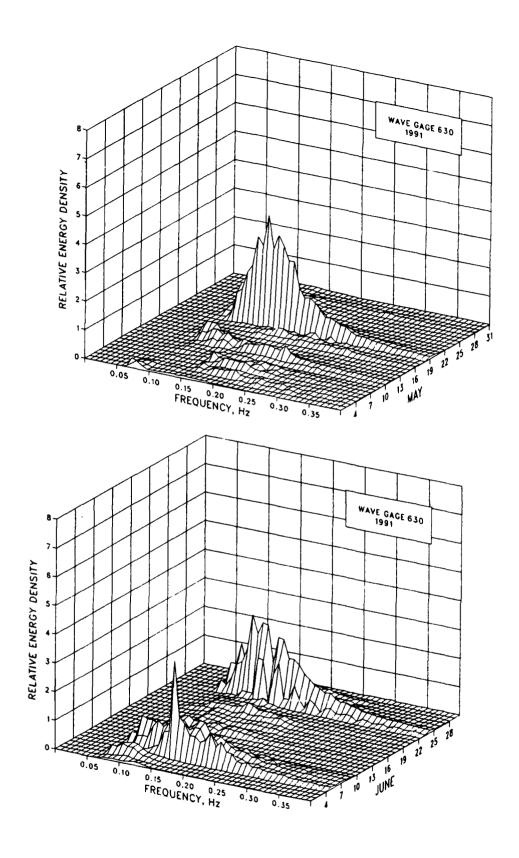


Figure B8. (Sheet 3 of 6)

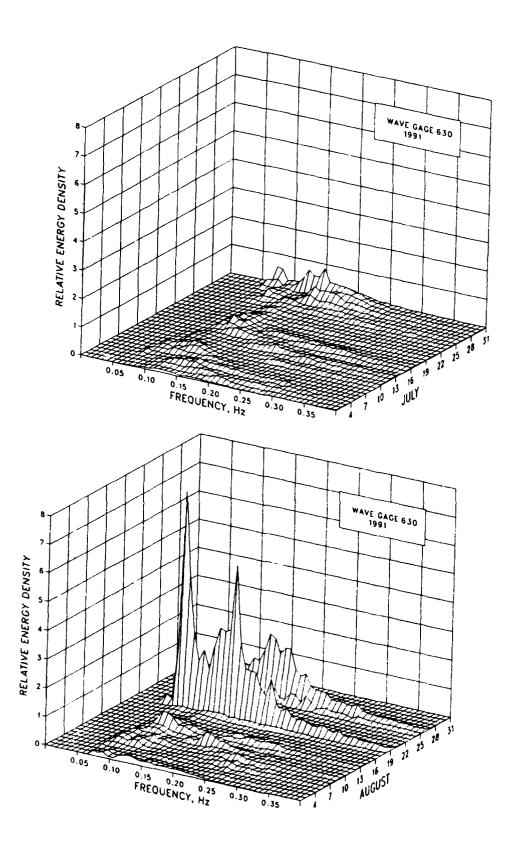


Figure B8. (Sheet 4 of 6)

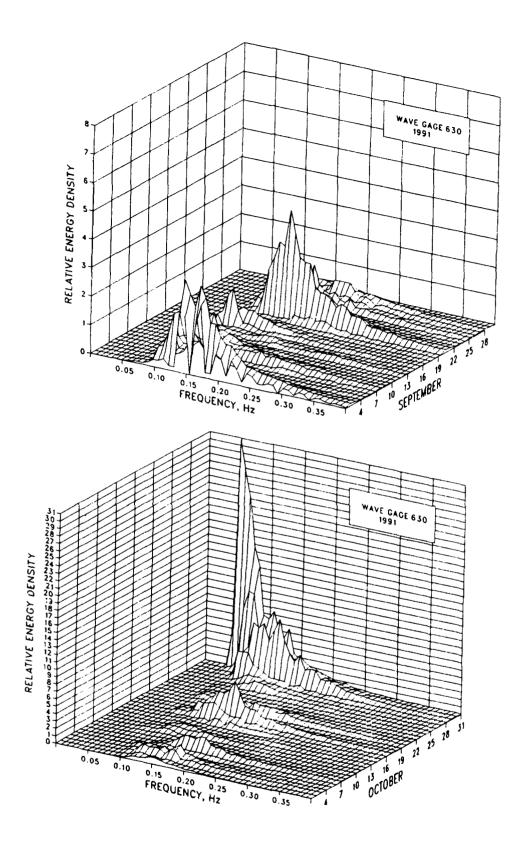


Figure B8. (Sheet 5 of 6)

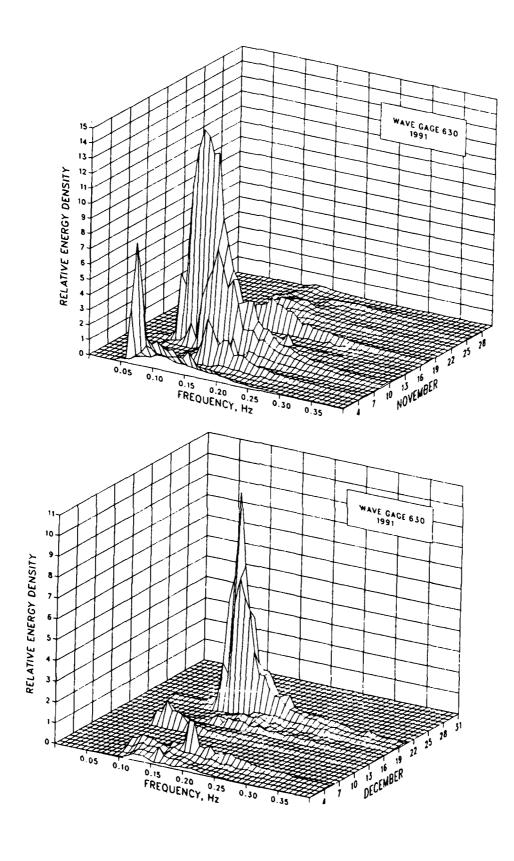


Figure B8. (Sheet 6 of 6)

Table B7
Wave Statistics for Gage 630

				1991				1980-1991									
		He	ight		Per	iod				ight		Per	iod				
		Std.				Std.			Std.				Std.				
	Mean	Dev.	Extreme		Mean	Dev.	Number	Mean	Dev.	Extreme		Mean	Dev.	Number			
Month	_m_	_ m	m	Date	sec	<u>sec</u>	Obs.	_ n	_m_	<u>m_</u>	<u>Date</u>	sec	sec_	Obs.			
Jan	1.5	0.7	3.2	9	8.0	2.5	61	1.2	0.7	4.5	1983	8.1	2.7	1255			
Feb	1.4	0.7	2.8	23	7.5	1.7	25	1.2	0.7	5.1	1987	8.4	2.6	1146			
Mar	1.2	0.5	2.1	30	9.2	2.4	118	1.2	0.7	4.7	1983	8.7	2.6	1358			
Apr	1.0	0.6	3.5	20	7.9	1.8	120	1.0	0.6	5.0	1988	8.6	2.6	1327			
May	0.8	0.5	2.6	19	7.8	2.9	122	0.9	0.5	3.3	1986	8.1	2.5	1351			
Jun	0.9	0.5	2.7	23	8.4	1.9	106	0.8	0.4	2.7	1991	7.8	2.2	1244			
Jul	0.7	0.2	1.3	30	7.8	2.1	116	0.7	0.3	2.1	1985	8.1	2.4	1280			
Aug	0.8	0.5	3.5	19	8.9	2.5	123	0.8	0.5	3.6	1981	8.2	2.5	1303			
Sep	1.1	0.5	2.6	1	8.1	1.7	119	1.1	0.6	6.1	1985	8.6	2.6	1310			
0ct	1.4	1.0	5.4	31	9.7	3.4	122	1.3	0.7	5.4	1991	8.8	2.8	1361			
Nov	1.1	0.9	4.6	9	8.2	2.9	118	1.1	0.7	4.6	1991	7.9	2.8	1155			
Dec	1.0	0.5	2.9	19	7.5	2.6	41	1.2	0.8	5.6	1980	8.2	2.9	1108			
Annual	1.1	0.6	5.4	0ct	8.3	2.6	1191	1.0	0.6	6.1	Sep 1985	5 8.3	2.6	15198			

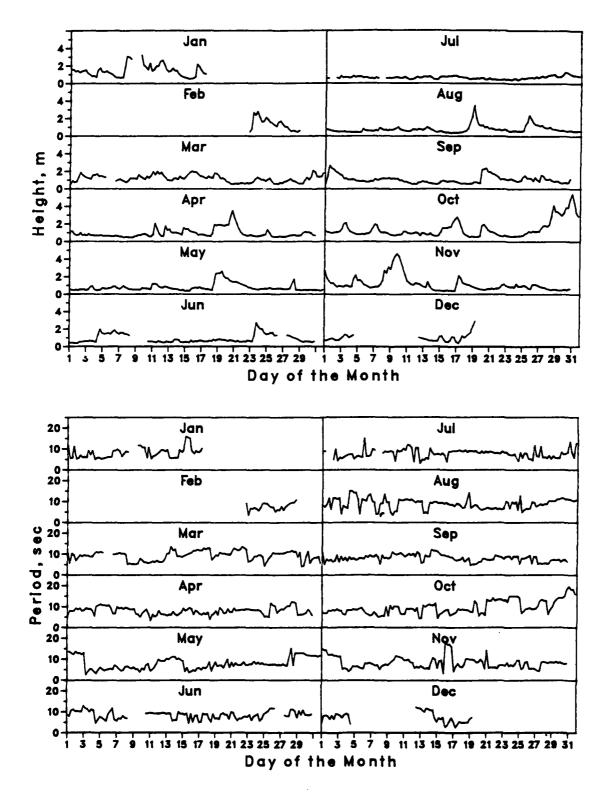


Figure B9. Time histories of wave height and period for Gage 630

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

Davis Highway, Soite 1204, Amington, VA 222		<u> </u>	ect (0704-0188), Washington, DC 20503.
1. AGENCY USE ONLY (Leave bla	June 1993	3. REPORT TYPE AND Final report	DATES COVERED
4. TITLE AND SUBTITLE			5. FUNDING NUMBERS
	1991 CERC Field Research Fa	rility:	3. 7 3.13.113
Volume I: Main Text and		,	
Volume II: Appendixes C	inrough E		
6. AUTHOR(S)			
Michael W. Leffler, Cliffor	rd F. Baron, Brian L. Scarboro	ugh,	
Kent K. Hathaway			WU 32525
7. PERFORMING ORGANIZATION	NAME(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION REPORT NUMBER
		:	
	ent Station, Coastal Engineerin	g Research Center	Technical Report
3909 Halls Ferry Road, Vic	ksburg, MS 39180-6199		CERC-93-9
9. SPONSORING/MONITORING A	GENCY NAME(S) AND ADDRESS(ES)	10. SPONSORING/MONITORING AGENCY REPORT NUMBER
			AGENCY REPORT NUMBER
US Army Come of Engine	Washington DC 20314 16	200	
US Army Corps of Enginee	ers, Washington, DC 20314-10	.w	
11. SUPPLEMENTARY NOTES			· · · · · · · · · · · · · · · · · · ·
See reverse.			
12a. DISTRIBUTION / AVAILABILITY	STATEMENT		12b. DISTRIBUTION CODE
			725. 5.5155
		•	
Approved for public release	u distribution is unlimited		
Approved for public release	, distribution is unfillited.		
13. ABSTRACT (Maximum 200 woi			
			de during 1991 at the US Army
Engineer Waterways Exper	iment Station (WES) Coastal E	ngineering Research C	enter's (CERC's) Field Research
Facility (FRF) in Duck, NC	. The report includes comparis	sons of the present year	r's data with cumulative statistics
from 1980 to the present.	•	• •	
	d oceanographic data monthly	hathymetric survey re	sults, samples of biannual aerial
			marized in this report. The year
			s with 6-m significant height and
	ere measured 6 km from shore		
			ted at the FRF that began with
			1979. These reports are available
from the WES Technical R	eport Distribution Section of th	e Information Technol	ogy Laboratory, Vicksburg, MS.
14. SUBJECT TERMS			15. NUMBER OF PAGES 210 (In two volumes)
			210 (in two volumes)
			16. PRICE CODE
See reverse.			
17. SECURITY CLASSIFICATION	18. SECURITY CLASSIFICATION	19. SECURITY CLASSIFIC	ATION 20. LIMITATION OF ABSTRACT
OF REPORT	OF THIS PAGE	OF ABSTRACT	
UNCLASSIFIED	UNCLASSIFIED		1

11. (Continued).

A limited number of copies of Volume II (Appendixes C through E) were published under a separate cover. Copies of Volume I (this report and Appendixes A and B) are available from the National Technical Information Service, 5285 Port Royal Road, Springfield, VA 22161.

14. (Continued).

Meterologic research--statistics (LC)
Oceanographic research--statistics (LC)
Oceanographic research stations--North Carolina--Duck (LC)
Water waves--statistics (LC)